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## **Time-dependent receiver extension for FWI: an alternative extension method for cycle skipping mitigation**

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# Time-dependent receiver extension for FWI: an alternative extension method for cycle skipping mitigation

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Running head: **Time-dependent receiver extension**

## ABSTRACT

Extension strategies for full waveform inversion (FWI) rely on introducing additional degrees of freedom to the FWI problem, which expands the search space. This search space extension helps relaxing the non-convexity of the problem, and thereby alleviating the cycle-skipping issue. Receiver-based extension strategy introduces the receiver position as the additional degree of freedom to full waveform inversion, in order to improve the fit between the observed and calculated data at early iterations. This helps circumvent the cycle-skipping phenomenon. In this study, we make this receiver position time-dependent, meaning that the receiver positions vary as a function of the acquisition time. The resulting mathematical problem is a two nested-loops minimization, where the outer loop is the conventional FWI loop to update the subsurface mechanical parameters, and the inner loop aims at finding the optimal time-dependent virtual receivers positions. This inner loop problem is heavily nonlinear and non-convex. Finding the global minimum is therefore a challenging task. We use for that a computational intelligence technique, Particle Swarm Optimization (PSO). PSO makes it possible to thoroughly explore the search space with few iterations. Numerical experiments using a North Sea exploration 2D synthetic model,

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4 28 starting from crude initial models, illustrate that the method is robust and is very easy to  
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## INTRODUCTION

Full waveform inversion (FWI) is a high resolution seismic imaging technique, which aims at reconstructing the subsurface parameters using the full seismic waveforms. From a mathematical standpoint, FWI is formulated as a partial differential equation (PDE) constrained optimization problem, where the optimality criterion is the fit between the observed and the calculated datasets. This constrained optimization problem is solved iteratively, using gradient based approaches. The synthetic data which are computed in a given initial model (using a wave equation operator), are conventionally compared to the observed data in the least-squares sense. That is, the  $L_2$  norm of the difference between the observed and synthetic datasets, which we call the misfit. The model is then updated in a manner that reduces this misfit. However, the  $L_2$  misfit function is non-convex, meaning that it contains numerous local minima. Therefore, gradient based (local) optimization strategies might fail to converge to a meaningful solution. This occurs when the initial model is not accurate enough, causing the calculated data to be shifted in time by more than half the dominant period, with respect to the observed data (Virieux and Operto, 2009). This time shift between the two datasets is driven by the long wavelength (smooth) part of the velocity model (Jannane et al., 1989). This long wavelength part of the model controls the kinematics of the seismic data. Starting from an initial velocity model that does not contain the correct long wavelength velocity structure, which gives rise to a time shift larger than half the dominant period, causes FWI to converge to a local minimum. This is the well-known cycle-skipping issue, and it stems from the oscillatory nature of the seismic data.

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51 Numerous strategies have been developed to circumvent this issue, such as multiscale  
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Numerous strategies have been developed to circumvent this issue, such as multiscale approaches. In this framework, the inversion can be performed from lower to higher frequencies (Bunks et al., 1995; Sirgue and Pratt, 2004), as starting from lower frequencies results in broader phases, the support of which is likely to overlap, decreasing the apparent shift between the observed and calculated data. The inversion can also be done from narrower to wider offsets (Shipp and Singh, 2002; Brossier et al., 2009), as the shorter the offset, the less is the time-shift. This can be done in combination with time-windowing, considering at first the earlier events, and increasing this time window when the frequency and offsets are increased, as the model estimate improves. These strategies, rely on the availability of low frequencies and large offset in the data, which is not always possible. Furthermore, they do require heavy human intervention, making the FWI process less automatic.

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More recent advances suggest different strategies to overcome the cycle-skipping issue, by reformulating the FWI problem. We divide these strategies into two categories. The first one relies on using alternative misfit functions, instead of the conventional  $L_2$  norm. The second introduces additional degrees of freedom to the FWI problem, to relax the non-convexity. The strategies that fall in the first category use different metrics to measure the distance between the observed and calculated data. These alternative misfit functions can exhibit improved convexity, compared with the  $L_2$  misfit function. They can be based on crosscorrelation (Luo and Schuster, 1991; van Leeuwen and Mulder, 2010), deconvolution (Luo and Sava, 2011; Guasch et al., 2019; Yong et al., 2022), instantaneous envelope (Bozdağ et al., 2011; Wu et al., 2014), dynamic time-warping (Ma and Hale, 2013) or

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4 73 optimal transport distances (Métivier et al., 2016, 2019; Yang et al., 2018b), to cite a few.  
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7 74 The second category encompasses strategies that rely on introducing additional degrees  
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10 75 of freedom to the FWI problem. This is done to help relaxing the non-convexity by fitting  
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12 76 the calculated data to the observed data, when the model estimate is poor. The strategy pre-  
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14 77 sented in this study belongs to this class of methods. The additional degrees of freedom can  
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17 78 be introduced in the model space, giving the so-called model extension strategies. These  
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19 79 methods rely on the assumption of scale separation between the background model and the  
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22 80 reflectivity model, in a similar fashion as reflection waveform inversion (RWI) methods  
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24 81 (Brossier et al., 2015; Yao et al., 2020). This is achieved during the image volume con-  
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27 82 struction, introducing horizontal subsurface offsets or time lags as the additional degrees of  
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29 83 freedom in the imaging condition. This depth oriented image construction workflow repre-  
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32 84 sents the so-called Migration Velocity Analysis (MVA) algorithms (Biondi and Sava, 1999;  
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34 85 Symes, 2008; Mulder, 2014), where it is potentially possible to fit the observed data in a  
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37 86 wrong background model. Similar to MVA, inversion velocity analysis introduces subsur-  
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39 87 face offsets or time lags as the additional degrees of freedom, using a nested optimization  
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42 88 approach (Biondi and Almomin, 2014; Chauris and Cocher, 2017; Barnier et al., 2023a,b).  
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44 89 An inner loop updates the reflectivity in a given background model in a migration process,  
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46 90 while the outer loop updates the background model according to some focusing criterion.  
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48 91 The additional degrees of freedom are relaxed during the process of FWI, thanks to the  
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50 92 use of a penalty term in the misfit function (an annihilator). The use of an annihilator is  
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53 93 common to all extension methods. When the extension is carried out in the model space,  
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55 94 it gives rise to high dimensional problems. For instance, model extension with sub-surface  
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4 95 offsets (the extended parameter) leads to 3D problem in the 2D case  $(x, y, h)$ ,  $h$  being the  
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6 96 horizontal subsurface offset. In 3D it leads to a 5D problem  $(x, y, z, h_x, h_y)$  (Chauris and  
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9 97 Cocher, 2017). The computation and storage related to these hypercubes can be prohibitive  
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11 98 for large scale 3D problems.  
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14 99 van Leeuwen and Herrmann (2013, 2016) introduced wavefield reconstruction inver-  
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17 100 sion (WRI), where the search space is extended by optimizing over both the wavefield  
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19 101 and the model parameters. This is achieved by considering the wave equation as a soft con-  
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22 102 straint, using a penalty method. The minimization of the misfit associated with this problem  
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24 103 gives rise to a linear system, which van Leeuwen and Herrmann (2013) call the augmented  
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27 104 wave equation. This augmented wave equation gathers the data extraction from the wave-  
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29 105 field constraint, and the wave equation. This is done in the frequency domain, because  
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31 106 one linear linear system replaces the classical wave equation, thanks to the possibility of  
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34 107 the wave equation operator factorization in the frequency domain. It is difficult to use this  
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37 108 formulation with explicit time-marching in the time-domain, where such factorization is  
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39 109 not possible. WRI is controlled by a penalty parameter, a scalar weight given to the penalty  
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41 110 term of the wave equation. The data is matched well for small values of the penalty param-  
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44 111 eter, even with poor velocity models (less importance is given to the wave equation). We  
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47 112 note that the penalty parameter needs to be increased during FWI iterations, which makes  
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49 113 the tuning difficult. This can be circumvented using an augmented Lagrangian formulation  
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51 114 instead of the penalty method (Aghamiry et al., 2018, 2019b,a), which they call Iteratively  
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53 115 Refined WRI (IR-WRI).  
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56 116 Source extension methods are obtained by reparametrizing the WRI by means of a  
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4 117 change of variables (Wang et al., 2017; Huang et al., 2018a). Through the change of vari-  
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6 118 ables, the reconstructed wavefield is replaced with the extended source (also referred to as  
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9 119 the wave equation error, or scattering source in the literature). The extended source may  
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11 120 contain energy away from the source position, when the velocity model is farther from the  
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14 121 target one, which allows to fit the observed data to the synthetic. Huang et al. (2018a) call  
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16 122 this method Matched Source Waveform Inversion (MSWI), and it is equivalent to WRI.  
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18 123 Similar to WRI, source extension methods are performed in frequency domain (Huang and  
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21 124 Symes, 2015; Huang et al., 2018a,b, 2019).

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24 125 A time-domain implementation of source extension methods was initially introduced  
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26 126 by Wang et al. (2017), which they achieve with a source extension approximation (their  
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28 127 equations 5 to 7). Aghamiry et al. (2020) introduced another method for source extension  
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31 128 using an explicit time-marching scheme, however it comes with a computational overhead,  
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34 129 which stems from the backward-forward time-stepping recursion they use. They argue that  
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36 130 this may be compensated for by the accelerated convergence, and the improved model pa-  
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38 131 rameters estimate accuracy. Gholami et al. (2022) propose a time-domain implementation  
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41 132 of IR-WRI, however it does not account for the data-domain Hessian (it is approximated by  
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43 133 a scaled identity matrix), which could be detrimental for complex geology, when starting  
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46 134 from a crude initial model. More recently, a new time-domain extended source FWI (ES-  
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48 135 FWI) implementation was introduced by Guo et al. (2024). ES-FWI does account for the  
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51 136 data-domain Hessian, by means of a matching filter approximation (Liu and Peter, 2018).  
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53 137 A comprehensive review of source extension is given by Huang et al. (2019), and more  
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55 138 recently by (Operto et al., 2023).

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4 139 Extended-receiver FWI is an alternative extension strategy, first introduced by Métivier  
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7 140 and Brossier (2022). It relies on adding the additional degree of freedom at the receiver  
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12 141 position, using a static relocalization strategy. Receiver extension is directly applicable to  
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17 142 time-domain FWI, and has shown promising results in realistic numerical settings. How-  
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22 143 ever, the method is able to fit only the most energetic arrival, because the relocalization  
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27 144 is static. The authors have also noticed a slow convergence of the method. In this study  
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32 145 we build on the work of Métivier and Brossier (2022), introducing more freedom to the  
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37 146 receiver position, using a time-dependent relocalization strategy. This is done to help ob-  
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42 147 tain better fit for more complex data, and accelerate the convergence. Our new method is  
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47 148 also directly applicable to time-domain FWI in a straightforward manner, and it is easy to  
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52 149 tune. Time-dependent receiver extension relies on solving many small optimization prob-  
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57 150 lems (one problem per receiver), whose misfit functions are not convex, requiring the use  
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60 151 of global optimization. The outline of the paper is as follows: a brief overview of conven-  
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65 152 tional FWI as well as the state of the art extended-receiver FWI are given. Then we explain  
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70 153 the time-dependent receiver extension, after which we discuss the underlying optimization  
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75 154 problem. We then present a set of numerical experiments using a North Sea exploration  
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80 155 scale synthetic model, providing an in-depth analysis of the sensitivity of our method to its  
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85 156 tuning parameters. We conclude with a discussion about various aspects.

## BACKGROUND

### 157 Full waveform inversion

158 Full waveform inversion is a PDE constrained optimization problem, where the fit be-  
 159 tween the observed and calculated data is improved by iteratively updating the model pa-  
 160 rameters. We write the FWI problem

$$\min_m f(m) = \min_m \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \int_0^T |d_{cal,s}[m](\mathbf{x}_r, t) - d_{obs,s}(\mathbf{x}_r, t)|^2 dt, \quad (1)$$

161 subject to

$$\begin{cases} A(m)u_s(\mathbf{x}, t) = b_s(\mathbf{x}, t) \\ d_{cal,s}[m](\mathbf{x}_r, t) = R_{s,r}u_s[m](\mathbf{x}, t), \end{cases} \quad (2)$$

162 where  $d_{obs,s}$  are the observed data, and  $d_{cal,s}$  are the calculated data.  $s$  and  $r$  are the source  
 163 and receiver indices, respectively,  $N_s$  is the total number of sources,  $N_r$  is the total number  
 164 of receivers, and  $\mathbf{x}_r$  is the position of the receiver  $r$ . The calculated data are extracted from  
 165 the wavefield  $u_s$ , which is computed using the wave equation operator  $A(m)$  (equation  
 166 2) with  $m$  being the model parameters vector, and  $b_s$  being the source term.  $R_{s,r}$  is the  
 167 restriction operator, which extracts the wavefield values at the receiver positions using a  
 168 convolution with a Dirac delta function

$$R_{s,r}u_s[m](\mathbf{x}, t) = \int_{\Omega} \delta(\mathbf{x} - \mathbf{x}_r)u_s[m](\mathbf{x}, t)d\mathbf{x}, \quad (3)$$

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4 where  $\delta(\mathbf{x})$  is the Dirac delta function and  $\Omega$  is the computation domain. The constrained  
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7 optimization problem (1) can be solved by finding the saddle-point of the associated La-  
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10 grangian (Haber et al., 2000). However, the computational cost of solving this problem  
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12 using local optimization for large scale problems is prohibitive: the simultaneous update  
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14 of the wavefields, the model parameters and the Lagrange multipliers requires their storage  
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17 in memory, which is infeasible for large scale problems. In practice, the following reduced  
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19 space approach is used

$$\min_m f(m) = \min_m \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \int_0^T |R_{s,r} A(m)^{-1} b_s(\mathbf{x}, t) - d_{obs,s}(\mathbf{x}_r, t)|^2 dt. \quad (4)$$

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28 Problem (4) is an unconstrained optimization problem, where the wavefield  $u_s$  has been  
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31 eliminated from the optimization variables, which exacerbates the non-linearity with re-  
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34 spect to the model parameters. Problem (4) is solved -iteratively- using local optimization  
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37 strategies (Nocedal and Wright, 2006). To do so, the gradient of the objective function  
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39 needs to be computed. The adjoint state strategy is used to carry out this computation  
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41 (Plessix, 2006). Following the adjoint state technique, the gradient is obtained using

$$\nabla_m f(m) = \sum_{s=1}^{N_s} \left\langle \frac{\partial A}{\partial m} u_s(\mathbf{x}, t), \lambda_s(\mathbf{x}, t) \right\rangle, \quad (5)$$

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50 where the notation  $\langle \bullet, \bullet \rangle$  indicates an inner-product operation. In time-domain FWI, it cor-  
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53 responds to the zero-lag cross-correlation between the weighted incident wavefield and the  
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60 adjoint wavefield. The latter is computed by back-propagating the data residuals (difference  
between the observed and calculated data) injected at the receivers positions, following

$$\begin{cases} A(m)^T \lambda_s(\mathbf{x}, t) = \sum_{r=1}^{N_r} R_{s,r}^T \mu_s[m](\mathbf{x}_r, t) \\ \mu_s[m](\mathbf{x}_r, t) = d_{cal,s}[m](\mathbf{x}_r, t) - d_{obs,s}(\mathbf{x}_r, t), \end{cases} \quad (6)$$

186 where  $\lambda_s$  is the adjoint field, computed backwards in time using the wave equation operator  
 187  $A^T(m)$ . The source term is the data residuals  $\mu_s$  injected at the receivers positions by the  
 188 operator  $R_{s,r}^T$ . Once the gradient is obtained, the model can be updated. In all the examples  
 189 we show in this paper, we use the preconditioned limited memory BFGS (*l-BFGS*) (Nocedal,  
 190 1980) algorithm. The new model  $m_{k+1}$  is therefore obtained by updating the model  
 191 at iteration  $k$  following

$$m_{k+1} = m_k - \alpha_k Q_k \nabla_m f(m_k), \quad (7)$$

192 where  $k$  is the iteration number,  $\alpha_k$  is a step-length obtained with a linesearch strategy  
 193 (Nocedal and Wright, 2006), and  $Q_k$  is the inverse Hessian approximation obtained with  
 194 the *l-BFGS* algorithm, using  $l$  previously stored gradients.

## 195 **Static receiver extension for FWI**

### 196 **Principle**

197 Receiver extension introduces the receiver position as an additional degree of freedom  
 198 (Métivier and Brossier, 2022). This additional degree of freedom allows to compensate  
 199 for the kinematic mismatch between the observed and calculated data. In other words, by  
 200 allowing the receiver to move in space, a fit can be obtained in the wrong medium velocity.

201 We write the receiver extension misfit function

$$\min_{m, \Delta x} \tilde{f}(m, \Delta x) = \min_{m, \Delta x} \frac{1}{2} \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \int_0^T |\tilde{d}_{cal,s}[m](\mathbf{x}_r + \Delta x_r, t) - d_{obs,s}(\mathbf{x}_r, t)|^2 dt + \alpha \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \mathcal{P}_{1,s}[\Delta x_r]. \quad (8)$$

202 Equation (8) is a bivariate misfit function, depending on  $m$  and  $\Delta x_r$ , the latter being  
 203 the additional degree of freedom, namely, the receiver relocation. The first term in the  
 204 right hand side is the data fit term, where  $\tilde{d}_{cal,s}$  are the calculated (extended) data, which  
 205 are extracted at the new receiver position. This new receiver position is shifted in space by  
 206 the quantity  $\Delta x_r$ . The calculated data are thus obtained following

$$\tilde{d}_{cal,s}[m](\mathbf{x}_r + \Delta x_r, t) = \int_{\Omega} \delta(\mathbf{x} - (\mathbf{x}_r + \Delta x_r)) u_s[m](\mathbf{x}, t) d\mathbf{x} \stackrel{\text{def}}{=} \tilde{R}_{s,r}[\Delta x_r] u_s[m](\mathbf{x}, t), \quad (9)$$

207 with  $\tilde{R}_{s,r}$  being the extended restriction operator. The operator  $\tilde{R}_{s,r}$  is similar to the con-  
 208 ventional FWI restriction operator  $R_{s,r}$ , however, the extraction is now performed at the  
 209 new receiver position  $\mathbf{x}_r + \Delta x_r$ ,  $\mathbf{x}_r$  being the true receiver position. The second term in the  
 210 right hand side of equation (8) is a penalty term, which controls the receiver extension, and  
 211  $\alpha$  is a tuning parameter. This term is used in order to prevent the relocation from being  
 212 too large. The expression of  $\mathcal{P}_{1,s}$  is given in appendix A.

213 We illustrate the leading idea behind the receiver extension with a simple numerical ex-  
 214 periment. In a homogeneous medium ( $v_{true} = 2000 \text{ m.s}^{-1}$ ) we consider one source/receiver

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4 215 couple. The observed trace is shown in a black dashed line in Figure 1b. The synthetic trace  
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6 216 is computed in a medium with a higher velocity ( $2300 \text{ m.s}^{-1}$ ), and it is shown in a red solid  
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9 217 line. By allowing the receiver to move (blue triangle in Figure 1a), the kinematic mismatch  
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11 218 between the observed and calculated data is eliminated, and the traces are aligned in time.  
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14 219 The extended (relocated) trace is shown in blue. We perform the same experiment for dif-  
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16 220 ferent velocities, and for different receiver relocalizations. This allows us to visualize the  
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18 221 objective function of equation (8), for each velocity and for each receiver position. This  
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21 222 is presented in Figure 2a, where the dashed black line shows the misfit variation at the  
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23 223 original receiver position (conventional FWI). This misfit is not convex. However, if we  
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26 224 take the minimum along the relocalization axis (the extended dimension) for each velocity  
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28 225 following the red line, a convex misfit function is obtained.

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32 226 [Figure 1 about here.]  
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36 227 [Figure 2 about here.]  
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## 41 228 **Computing a numerical solution**

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45 229 Bivariate misfit functions such as equation (8), are usually minimized using nested-  
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48 230 loops strategy. The outer loop is the conventional FWI optimization over the model pa-  
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50 231 rameters  $m$ . The inner-loop solves the sub-problem of finding the optimal receiver relo-  
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52 232 calization  $\Delta x$  for a given model  $m$  (we drop the subscripts  $s$  and  $r$  in this analysis for  
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55 233 compactness). Consider the bivariate objective function  $f(m, \Delta x)$  and the minimization  
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57 234 problem  
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$$\min_{m, \Delta x} f(m, \Delta x), \quad (10)$$

where  $m$  is the model parameters vector and  $\Delta x$  is the receiver relocalization (a spatial shift). This problem is equivalent to

$$\min_m \hat{f}(m) \quad (11)$$

where we eliminate the variable  $\Delta x$  using

$$\hat{f}(m) = f(m, \overline{\Delta x(m)}), \quad (12)$$

with

$$\overline{\Delta x(m)} = \operatorname{argmin}_{\Delta x} f(m, \Delta x). \quad (13)$$

The objective function  $\hat{f}(m)$  is minimized in the outer loop (equation 11), while the inner loop carries out the minimization shown in equation (13) which defines  $\Delta x(m)$ . The inner loop aims at finding the optimal relocalization  $\Delta x$  for a given model iterate. In the framework of FWI, the gradient of the outer loop misfit function  $\hat{f}(m)$  is required. This gradient is obtained following

$$\nabla_m \hat{f}(m) = \frac{\partial f(m, \overline{\Delta x(m)})}{\partial m} + \frac{\partial f(m, \overline{\Delta x(m)})}{\partial \Delta x} \frac{\partial \overline{\Delta x}}{\partial m}. \quad (14)$$

Per equation (12),  $\overline{\Delta x}$  is a minimizer of  $f(m, \Delta x)$  with respect to  $\Delta x$ , therefore, the

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4 first order optimality conditions tell us that  
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$$\frac{\partial f(m, \overline{\Delta x(m)})}{\partial \Delta x} = 0, \quad (15)$$

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14 which yields

$$\nabla_m \hat{f}(m) = \frac{\partial f(m, \overline{\Delta x(m)})}{\partial m}. \quad (16)$$

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20 Equation (16) shows that the gradient of the outer misfit function around  $m$ , is equal to  
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23 the gradient with respect to  $m$  of the bivariate misfit function  $f(m, \Delta x)$  calculated at  $\overline{\Delta x}$ .  
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25 The gradient is obtained following  
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$$\nabla_m \tilde{f}(m) = \sum_{s=1}^{N_s} \left\langle \frac{\partial A}{\partial m} u_s[m](\mathbf{x}, t), \lambda_s[m, \overline{\Delta x}](\mathbf{x}, t) \right\rangle, \quad (17)$$

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34 where the adjoint field  $\lambda_s$  is obtained using  
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$$\begin{cases} A(m)^T \lambda_s[m, \overline{\Delta x}](\mathbf{x}, t) = \sum_{r=1}^{N_r} \tilde{R}_{s,r}^T[\overline{\Delta x_r}] \tilde{\mu}_s[m](\mathbf{x}_r + \overline{\Delta x_r}, t) \\ \tilde{\mu}_s[m](\mathbf{x}_r + \overline{\Delta x_r}, t) = \tilde{d}_{cal,s}[m](\mathbf{x}_r + \overline{\Delta x_r}, t) - d_{obs,s}(\mathbf{x}_r, t). \end{cases} \quad (18)$$

39  
40  
41  
42  
43  
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45  
46 This means that the calculated data are now extracted at the extended receiver position  
47  
48  
49 per equation (9), and the adjoint source position corresponds to the extended receiver as  
50  
51 well. The latter is achieved using  $\tilde{R}_{s,r}^T$ , where the extended data residuals  $\tilde{\mu}_s$  are injected at  
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54 extended receiver positions. Throughout this paper, we use  $\tilde{\bullet}$  to indicate extended quanti-  
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56 ties.  
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 4 256 The extended receiver strategy with the nested-loops is summarized in algorithm 1. A  
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 6  
 7 257 forward modeling is performed in a given model, then the inner-loop computation provides  
 8  
 9 258 the optimal receiver relocalizations. The extended calculated data are then extracted at the  
 10  
 11 259 extended receiver positions. The model is then updated using gradient based optimization.  
 12  
 13  
 14 260 It is crucial to note that the inner-loop computation does not require performing forward  
 15  
 16 261 simulations, the extended data are simply extracted from the already computed incident  
 17  
 18 262 wavefield. Métivier and Brossier (2022) use a grid-search to solve the inner loop problem.  
 19  
 20  
 21 263 Indeed, finding one optimal receiver relocalization per receiver can be easily (and quickly)  
 22  
 23  
 24 264 obtained with this global optimization scheme.

---

**Algorithm 1** Nested loop optimization

---

```

27 while  $\hat{f}(m_k) > \epsilon_{outer}$  do
28    $u_s \leftarrow do\_forward\_modelling(m)$ 
29   while  $f(m_k, \Delta x) > \epsilon_{inner}$  do
30      $f(m_k, \Delta x) \leftarrow compute\_inner\_cost(u_s)$ 
31   end while
32    $\overline{\Delta x} \leftarrow \Delta x$ 
33    $\hat{f}(m_k) \leftarrow f(m_k, \overline{\Delta x})$ 
34    $m_k \leftarrow update\_model(m_{k-1}, \overline{\Delta x}, u_s)$ 
35    $k \leftarrow k + 1$ 
36 end while

```

---

265 **Limitations of static receiver-extension**

46  
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 48  
 49  
 50 266 The extended-receiver FWI of Métivier and Brossier (2022) uses static relocalization,  
 51  
 52 267 that is, the receiver position does not depend on time. Despite the promising results, the  
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 54  
 55 268 analysis was performed in the framework of a single arrival. They also observed that the  
 56  
 57 269 method suffers from a slow convergence rate. We aim in the present study at addressing  
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4 270 these two main issues. Our first investigation step is to introduce more degrees of freedom,  
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6  
7 271 in order to allow the receiver to move as a function of the acquisition time, as such a fit  
8  
9 272 for more complex data can be obtained. By obtaining a better fit at earlier iterations, the  
10  
11 273 convergence could be accelerated. This is carefully analyzed and illustrated in the present  
12  
13  
14 274 paper.

15  
16  
17 275 Before going into the formalism and the implementation details, we illustrate this strat-  
18  
19 276 egy with a simple numerical experiment. We consider a two arrivals case, a transmitted  
20  
21  
22 277 and a reflected arrival. The observed data are simulated in a two layers medium, the first  
23  
24 278 layer with  $v_p = 2000 \text{ m.s}^{-1}$ , and a second layer with  $v_p = 3500 \text{ m.s}^{-1}$  (Figure 3). For the  
25  
26  
27 279 sake of illustration, we choose a two layers starting model, where the first layer velocity is  
28  
29 280 faster, at  $2500 \text{ m.s}^{-1}$ , while the second layer velocity is the true one ( $v_p = 3500 \text{ m.s}^{-1}$ ).  
30  
31 281 The observed trace is shown in a dashed black line, and the calculated trace in a solid blue  
32  
33  
34 282 line. The receiver relocalization as a function of time is shown in red (Figure 4). This curve  
35  
36 283 indicates the receiver relocalization value at each time step, we refer to this curve as the  
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38  
39 284 relocalization profile. Using receiver-extension, only one arrival can be fitted. This occurs  
40  
41 285 since the second (reflected) arrival would require another relocalization value in order to  
42  
43  
44 286 align it with the observed reflected arrival. Therefore, only the most energetic arrival is fit-  
45  
46 287 ted. Using time-dependent receiver extension (Figure 4c), a fit of both arrivals is obtained.  
47  
48 288 We show the FWI kernels in Figure 5, for conventional FWI, static and time-dependent  
49  
50  
51 289 receiver extension. The kernel for the conventional FWI case suggests a positive velocity  
52  
53 290 update (negative gradient), to a velocity that is already higher than the true value, in the first  
54  
55  
56 291 Fresnel zone (yellow arrows). With the static relocalization a correct velocity update is ob-

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5 292 tained in the first Fresnel zone, however two migration isochrones can be seen (red arrows),  
6  
7 293 and the rabbit ears (blue arrows) suggest a positive velocity update. This is caused by the  
8  
9 294 wrong fit of the second arrival (the adjoint source in Figure 5e shows two events related  
10  
11 295 to the reflection). Using time-dependent receiver-extension makes it possible to fit both  
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13  
14 296 arrivals, obtaining the correct velocity update also in the rabbit-ears Fresnel zones. We also  
15  
16  
17 297 see a single migration isochrone, thanks to the fit of the second arrival. This time-dependent  
18  
19 298 receiver-extension strategy is detailed in the next section.

20  
21  
22 299 [Figure 3 about here.]

23  
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26 300 [Figure 4 about here.]

27  
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29  
30 301 [Figure 5 about here.]

## 31 32 33 34 35 **TIME-DEPENDENT RECEIVER EXTENSION FOR FWI**

### 36 37 38 39 302 **Formalism**

40  
41  
42  
43 303 We write the new extended-receiver FWI misfit function as

$$\begin{aligned}
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48  
49 \min_{m, \Delta x(t)} \tilde{f}(m, \Delta x(t)) &= \min_{m, \Delta x(t)} \frac{1}{2} \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \int_0^T |\tilde{d}_{cal,s}[m](\mathbf{x}_r + \Delta x_r(t), t) - d_{obs,s}(\mathbf{x}_r, t)|^2 dt \\
 50  
51  
52  
53  
54  
55 &+ \alpha \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \mathcal{P}_{1,s}[\Delta x_r(t)] + \beta \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \mathcal{P}_{2,s}[\Delta \dot{x}_r(t)]. \\
 56  
57  
58 & \tag{19}
 \end{aligned}$$

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4 304 We aim at minimizing the bivariate misfit function in equation (19), where  $m$  are the  
5  
6 305 model mechanical parameters, and  $\Delta x_r(t)$  is now the time-dependent receiver relocaliza-  
7  
8 306 tion. The first term in equation (19) is the data fit term, which is the  $L_2$  norm of the data  
9  
10 307 residuals. The calculated data are obtained using equation (9) however, the receiver posi-  
11  
12 308 tion is now time-dependent. We write the new extended restriction operator  
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$$\tilde{R}_{s,r}[\Delta x_r(t)]u_s[m](\mathbf{x}, t) = \int_{\Omega} \delta(\mathbf{x} - (\mathbf{x}_r + \Delta \mathbf{x}_r(t)))u_s(\mathbf{x}, t)dx, \quad (20)$$

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23 309 where  $\Delta x_r(t)$  is the time-dependent receiver relocalization. The calculated data are ex-  
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25 310 tracted at the virtual receivers positions  $(\mathbf{x}_r + \Delta x_r(t))$  from the wavefield  $u_s(\mathbf{x}, t)$ . The  
26  
27 311 term  $\mathcal{P}_{1,s}$  in the right hand side of equation (19) penalizes the receiver relocalization, in or-  
28  
29 312 der to prevent it from being too large, and to force it to become small along iterations. The  
30  
31 313 parameter  $\alpha$  is a tuning parameter, which weighs this penalty term. Similarly, the term  $\mathcal{P}_{2,s}$   
32  
33 314 in the right hand side of equation (19) penalizes the receiver speed (the first order derivative  
34  
35 315 with respect to time of the receiver relocalization), and  $\beta$  is a tuning parameter. This term  
36  
37 316 is needed in order to mitigate potential Doppler effects, which stem from a moving receiver  
38  
39 317 during the calculated data extraction, and also from a moving adjoint source during the ad-  
40  
41 318 joint simulation. The interested reader is referred to the discussion part of this paper. The  
42  
43 319 full expressions of  $\mathcal{P}_{1,s}$  and  $\mathcal{P}_{2,s}$  can be found in appendix A. The adjoint field is obtained  
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45 320 using the adjoint system  
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$$\begin{cases} A(m)^T \lambda_s[m, \overline{\Delta x(t)}](\mathbf{x}, t) = \sum_{r=1}^{N_r} \tilde{R}_{s,r}^T[\overline{\Delta x_r(t)}] \tilde{\mu}_s[m](\mathbf{x}_r + \overline{\Delta x_r(t)}, t), \\ \tilde{\mu}_s[m](\mathbf{x}_r + \overline{\Delta x_r(t)}, t) = \tilde{d}_{cal,s}[m](\mathbf{x}_r + \overline{\Delta x_r(t)}, t) - d_{obs,s}(\mathbf{x}_r, t). \end{cases} \quad (21)$$

321 We observe that now the adjoint source moves as a function of the acquisition time.

322 The gradient is obtained following the adjoint state strategy

$$\nabla_m \tilde{f}(m) = \sum_{s=1}^{N_s} \left\langle \frac{\partial A}{\partial m} u_s[m](\mathbf{x}, t), \lambda_s[m, \overline{\Delta x(t)}](\mathbf{x}, t) \right\rangle. \quad (22)$$

323 As in the static case, the time-dependent strategy uses the nested-loops optimization  
 324 approach. The inner-loop finds the optimal receiver relocalizations, while the outer-loop  
 325 updates the model physical parameters. We now focus on the inner loop solution, starting  
 326 with the question: how to parametrize the time-dependent receiver relocalization  $\Delta x_r(t)$ ?

## 327 **Parametrization**

328 We seek to answer two questions: [1] how should we parametrize a receiver relocal-  
 329 ization that depends on the acquisition time? [2] how should we parametrize the receiver  
 330 motion in the physical space?

331 *Temporal parametrization*

332 One possible choice of parametrization is assigning a receiver relocalization to each  
 333 time step. However, this would give rise to a problem with a large number of degrees  
 334 of freedom (the number of time steps), which is prohibitive for the global optimization  
 335 strategies, that is going to be used to solve the inner loop problem. To keep a minimal  
 336 parametrization, we propose a piecewise polynomial interpolation. The time vector is  
 337 divided into segments, each of which contains one Lagrange polynomial. We write the  
 338 receiver relocalization as a function of the acquisition time

$$\Delta x(t) = \sum_{j=1}^{n_s} \sum_{k=1}^{N_\ell} a_{k+N_\ell \times (j-1)} \ell_k^{N_\ell}(t), \quad (23)$$

339 where  $\ell_k^{N_\ell}(t)$  are Lagrange basis functions of order  $N_\ell$ ,  $n_s$  is the number of segments and  
 340  $a_i$  ( $i = k + N_\ell \times (j - 1)$ ) are the values at the control points. In the inner loop we aim  
 341 at finding the optimal  $a_i$  values, that define the time-dependent virtual receivers positions.  
 342 We illustrate in Figure 6, using three segments with first order Lagrange polynomials. The  
 343 time-dependent relocalization is shown in black line plot, and the blue circles indicate  
 344 the control points. The unknowns for the receiver relocalization subproblem are therefore  
 345  $a = (a_1, a_2, \dots, a_{N_\ell \times n_s + 1})^T$ , we rewrite the minimization problem of equation (19) as

$$\min_{m,a} \tilde{f}(m, a), \quad (24)$$

346 which we solve using the same nested loops approach described in algorithm 1.

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347 [Figure 6 about here.]

348 *Spatial parametrization*

349 Métivier and Brossier (2022) use only horizontal relocalization, that is the receivers  
350 are allowed to move only following the horizontal axis, moving closer or farther from the  
351 source. In our case, relying solely on horizontal relocalization might not be advisable.  
352 This can be shown by a simple ray theory analysis (Benziane et al., 2023), to visualize the  
353 receiver positions which allow to fit transmitted and reflected arrivals. We consider a one  
354 layer over a half-space model (Fig. 7a). The travel-time expression of the reflected arrival  
355 in the true velocity model  $v_0$  is

$$T_0^2 = \frac{x^2}{v_0^2} + \frac{4z^2}{v_0^2}, \quad (25)$$

356 where  $x$  is the offset and  $z$  is the receiver vertical distance to the reflector. To obtain the  
357 same arrival time in a wrong velocity model  $v_1$ , the receiver is relocated. We introduce the  
358 quantities  $\Delta x$  and  $\Delta z$  which provide the same arrival time

$$T_0^2 = \frac{(\Delta x + x)^2}{v_1^2} + \frac{(\Delta z + 2z)^2}{v_1^2}. \quad (26)$$

359 Equating equations (25) and (26) gives

$$(\Delta x + x)^2 + (\Delta z + 2z)^2 = (4z^2 + x^2) \frac{v_1^2}{v_0^2}. \quad (27)$$

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4 360 Similarly, we perform the analysis for a transmitted arrival. The travel-time expression  
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7 361 of the transmitted arrival in the true velocity model  $v_0$  is  
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$$11 \quad T_0^2 = \frac{x^2}{v_0^2}. \quad (28)$$

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16 362 To obtain the same travel-time for the transmitted arrival in a wrong velocity model, the  
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19 363 receiver is relocated

$$20 \quad T_0^2 = \frac{\Delta z^2}{v_1^2} + \frac{(\Delta x + x)^2}{v_1^2}. \quad (29)$$

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27 364 Equating equations (28) and (29) gives

$$28 \quad (\Delta x + x)^2 + \Delta z^2 = x^2 \frac{v_1^2}{v_0^2}. \quad (30)$$

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37 365 Equations (27) and (30) are conic section equations. For the reflection case, equation  
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40 366 (27) describe a circle with a center  $(-x, -2z)$ , which is the source image with respect to the  
41  
42 367 reflector. The radius of this circle is  $\sqrt{(4z^2 + x^2) \frac{v_1^2}{v_0^2}}$ . We plot the solution of equation (27)  
43  
44 368 using different velocities,  $v_1 = 1500 \text{ m.s}^{-1}$ ,  $v_1 = v_0 = 1500 \text{ m.s}^{-1}$  and  $v_1 = 2500 \text{ m.s}^{-1}$ .  
45  
46  
47 369 The possible receiver positions that give the same travel-time fall on a circle, the radius  
48  
49 370 of which increases as the velocity increases. By allowing the receiver to move only hor-  
50  
51 371 izontally, a fit cannot be obtained for the lower velocity case (crosses "×" in Figure 7b).  
52  
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54 372 Similar to the reflected arrival case, equation (30) describes a circle. However, it is centered  
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56  
57 373 at the source position  $(-x, 0)$ . We plot the solution to our equation using three different

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4 374 velocities (Figure 7c). We observe that moving the receiver horizontally, makes it possible  
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7 375 to fit the transmitted arrival, for all velocities.

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10 376 By forcing the receiver to move towards the source following a  $\frac{\pi}{4}$  angle with respect  
11  
12 377 to the horizontal axis, a fit of the reflected and transmitted arrivals can be obtained. This  
13  
14 378 is achieved by simply equating  $\Delta x$  to  $\Delta z$  when the receiver moves towards the source.  
15  
16  
17 379 Therefore,  $\Delta z$  can be obtained from  $\Delta x$  using

$$\Delta z = \begin{cases} |\Delta x| & \text{if the receiver is moving towards the source} \\ 0 & \text{otherwise.} \end{cases} \quad (31)$$

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27  
28 380 This is the choice of parametrization that we make, in order to keep the parametrization  
29  
30 381 minimal. Again, allowing the receiver to move freely in all the spatial dimensions, would  
31  
32 382 give rise to an expensive inner-loop computation. This is avoided thanks to our spatial  
33  
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35 383 parametrization.

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39 384 [Figure 7 about here.]  
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43 385 We illustrate this parametrization with a numerical experiment, using the same setup as  
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45 386 in Figure 3. However, we use now a top layer velocity with a lower velocity. Because the  
46  
47 387 starting velocity is lower than the true one, the receiver needs to move towards the source.  
48  
49 388 If the receiver moves only horizontally, a fit for the reflected arrival cannot be obtained.  
50  
51  
52 389 This is shown in Figure 8a, where the observed data are shown in a black dashed line, and  
53  
54  
55 390 the extended calculated data are shown in a blue solid line. The receiver needs to move  
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57 391 following the  $z$ -axis in order to obtain a fit for the second arrival. This is in agreement with  
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4 392 our ray theory analysis. By allowing the receiver to move vertically (equation 31), a fit for  
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7 393 the reflected arrival is obtained.  
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10 394 [Figure 8 about here.]  
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## 16 INNER LOOP OPTIMIZATION

### 17 18 19 395 Overview

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23 396 The solution of the inner loop problem using our time-dependent receiver extension  
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26 397 raises a challenging optimization problem. We illustrate this using a North Sea exploration  
27  
28 398 scale synthetic model (Figure 9). We consider a single source/receiver couple, and a single  
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30 399 segment with first order Lagrange polynomial, leading to two control points  $a_1$  and  $a_2$ . We  
31  
32  
33 400 compute the inner-loop misfit function map, using a fine discretization of  $a_1$  and  $a_2$ , which  
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35  
36 401 we present in Figure 10. Not only our misfit function contains numerous minima: some  
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38 402 local minima may have very close values (Figure 10b). This makes finding the global min-  
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40  
41 403 imum a challenging task. A solution can be obtained using global optimization strategies.  
42  
43 404 However, it appears not tractable to solve the inner problem using grid-search optimization,  
44  
45  
46 405 as the size of this inverse problem will grow large with the time-dependence. Even with  
47  
48 406 the parametrization used for the present example (two control points), as the optimization  
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51 407 needs to be performed for all receivers. Our investigations on global optimization strategies  
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53 408 have led us to the choice of Particle Swarm Optimization (PSO) (Kennedy and Eberhart,  
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55 409 1995), over Markov-chain Monte Carlo (MCMC) (Aster et al., 2013) and Very Fast Sim-  
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57 410 ulated Annealing (VFSA) (Ingber, 1993). The former requires a large number of misfit  
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4 411 function evaluations to convergence to a good solution, while the latter suffers from pre-  
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6 412 mature convergence towards bad solutions. PSO on the other hand, allows for a thorough  
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9 413 exploration of the search space, with reasonable cost. The interested reader is referred to  
10  
11 414 the discussion part of the paper.  
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15 [Figure 9 about here.]  
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19 416 [Figure 10 about here.]  
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## 24 417 **Particle Swarm Optimization (PSO)**

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28 418 Particle Swarm Optimization is a computational intelligence technique, proposed by  
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31 419 Kennedy and Eberhart (1995). It is a heuristic optimization method where the search space  
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33 420 is explored by so-called particles, in order to minimize some misfit function  $g(\mathbf{x})$   
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$$39 \min_{\mathbf{x}} g(\mathbf{x}). \quad (32)$$

40  
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43 421 A swarm contains  $N_p$  particles, and each particle  $j$  explores the search space by its  
44  
45 422 position  $\mathbf{x}_j$ . The best model from the swarm (from all the particles), associated with the  
46  
47 423 lowest  $g(\mathbf{x})$  value, is referred to as the global best ( $\mathbf{x}_g$  in the equations below). The personal  
48  
49 424 best ( $\mathbf{x}_{p,j}$  in the equations hereafter) on the other hand, is the best solution obtained for each  
50  
51 425 individual particle. Let  $\mathbf{x}_j^i$  denotes a particle  $j$  position in a search space  $\mathbb{R}^N$  at iteration  $i$ .  
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55 426 The particle position is then updated to iteration  $i + 1$  as such  
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$$\mathbf{x}_j^{i+1} = \mathbf{x}_j^i + \mathbf{u}_j^{i+1}, \text{ with } \mathbf{x}_j^0 = U(\mathbf{x}_{min}, \mathbf{x}_{max}), \quad (33)$$

where  $\mathbf{u}_j^i$ , is the particle position update at iteration  $i$ . The starting particle positions are harvested from a uniform distribution ( $U$  in equation (33), where  $\mathbf{x}_{min}$  and  $\mathbf{x}_{max}$  are the search space bounds). In the literature,  $\mathbf{u}^i$ , is referred to as the particle speed, and is computed as

$$\mathbf{u}_j^{i+1} = \omega \mathbf{u}_j^i + c_1 \mathbf{r}_1^i : [\mathbf{x}_{p,j}^i - \mathbf{x}_j^i] + c_2 \mathbf{r}_2^i : [\mathbf{x}_g^i - \mathbf{x}_j^i]. \quad (34)$$

The first term in the right hand side is called the inertia term, it controls the contribution from the past iteration, with  $\omega$  being the inertia weight (typically  $\omega \in [0.9, 1.2]$ ). The second term in the right hand side is the contribution of the best position for each particle, where  $\mathbf{x}_{p,j}^i$  is the best personal position for a particle  $j$  along its past trajectory. The third term in the right hand side is the contribution of the global best position of the swarm, where  $\mathbf{x}_g^i$  is the global best position. Terms  $\mathbf{r}_1^i$  and  $\mathbf{r}_2^i$  are random variables vectors of the same dimension as the particle position  $\mathbf{x}_j^i$ , which are harvested from a uniform distribution.  $c_1$  and  $c_2$  are constants, usually set to equal values, and  $\mathbf{a} : \mathbf{b}$  denotes the term to term product of vectors  $\mathbf{a}$  and  $\mathbf{b}$ . If we wish to give more weight to either component, the constants  $c_1$  and  $c_2$  may be adjusted accordingly. This is the basic form of global best PSO (Engelbrecht, 2007).

## 442 Numerical example

443 In order to showcase PSO, we carry out a simple numerical test using the same example  
444 we showed earlier (Figure 9). We run PSO using 16 particles. We show snapshots of the  
445 swarm configuration at iterations 1, 40, 80 and 160 in Figure 11. The particles are shown in  
446 black, the personal best in red, the global best in magenta and the global solution which we  
447 obtain using a grid search is shown as a red star. The personal best positions are initialized  
448 with the particle positions and are updated at each iteration. The global best is selected  
449 from the personal bests (the particle whose personal best has the lowest cost). This process  
450 is repeated until convergence or the max number of iterations is reached. Note that none  
451 of the starting particles positions is near the global minimum, nonetheless, PSO manages  
452 to converge fairly quickly. As is clear from Figure 10, our misfit does contain many sec-  
453 ondary minima, which is why a population based optimization is a good choice. It allows  
454 for a thorough exploration of the search space. Even though the global-best is already on  
455 the global minimum, other particles still search in the vicinity of other secondary minima,  
456 thanks to the inertia term (equation 34). PSO can achieve convergence fairly quickly, how-  
457 ever, setting the maximum number iterations to a small value for all receivers is not a good  
458 idea. Indeed, convergence to a good solution is not guaranteed for the same number of iter-  
459 ations, for all receivers. A flexible way of handling this, is the use of what we call stalling  
460 detection. If the global best does not move in  $n_{stall}$  iterations the PSO is stopped, as we  
461 assume the global minimum has been reached. This helps to save computational time. For  
462 the first example (Figure 11), the max number of iterations is set to 400 and  $n_{stall} = 200$ .  
463  $n_{stall}$  is particularly high in this example because the swarm is small ( $N_p = 16$ ). For a

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4 464 larger swarm, stalling is observed earlier. For  $N_p = 16$  the global best has indeed ceased to  
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6  
7 465 change from the 275<sup>th</sup> iteration. However the optimization did not stop in this case, because  
8  
9 466 the global best needs to stall for 200 iterations. Next, we increase the number of particles  
10  
11 467 to  $N_p = 32$ , in order to observe the impact of the swarm size on the convergence (Figure  
12  
13  
14 468 12). Indeed, increasing the swarm size, leads to a sooner stalling, therefore a better conver-  
15  
16 469 gence. With 32 particles (shown in blue), stalling occurs at 127 iterations, PSO has stopped  
17  
18  
19 470 at 327 iterations. When using 64 particles (shown in red), the global best did not change  
20  
21 471 after 34 iterations, PSO was stopped at 234 iterations in this case. Better convergence is  
22  
23 472 obtained with a larger swarm size, because increasing the number of particles, allows for a  
24  
25  
26 473 better exploration of the search space. In other words, at each iteration, a larger swarm has  
27  
28 474 a better "view" of the search space. It is clear that the swarm size is an important parameter.  
29  
30  
31 475 In the literature a choice of  $\approx 30$  particles is common. A choice of too few particles reduces  
32  
33 476 the exploration abilities of the swarm, and choosing too many particles –although better in  
34  
35 477 terms of convergence– requires more cost function evaluations (Luu et al., 2018). In our  
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38 478 work, a swarm size is adapted based on the inner-loop parametrization. Higher dimensional  
39  
40 479 problems would benefit from a larger swarm. All the tests performed in this paper (unless  
41  
42  
43 480 otherwise stated) use 45 particles. As for the choice of the PSO parameters, we use the  
44  
45 481 results from Pedersen (2010). We set  $c_1 = -0.6485$ ,  $c_2 = 2.6475$  and  $\omega = -0.6485$ .

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49 482 [Figure 11 about here.]

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53 483 [Figure 12 about here.]

## APPLICATION TO A NORTH SEA EXPLORATION SCALE

### SYNTHETIC 2D MODEL

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11 484 For all our testing, we use the SEISCOPE (acoustic and visco-acoustic) modeling and  
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13 485 FWI engine TOYxDAC\_TIME (Yang et al., 2018a). The modeling is performed using  
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15 486 fourth order finite-differences, with staggered grids (Virieux, 1986; Levander, 1988). A  
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18 487 second order leap-frog scheme is used for the time-marching. We use Convolutional Per-  
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20 488 fectly Matched Layers (CPML) (Komatitsch and Martin, 2007) as absorbing boundary con-  
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22 489 ditions, in order to simulate an infinite medium. We note however that we do not enable  
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25 490 CPML when attenuation is used, instead, we use sponge layers (Cerjan et al., 1985). The  
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28 491 gradient computation is performed using the time-decimated incident wavefield, which is  
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30 492 saved solely at the boundary of the computation domain. This wavefield is interpolated  
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32 493 using Kaiser-windowed sinc interpolator (Yang et al., 2016c), and is propagated from the  
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35 494 boundaries during the adjoint simulation. When an attenuating medium is used, we employ  
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37 495 Checkpointing Assisted Reverse-Forward Simulation or CARFS (Yang et al., 2016b). We  
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40 496 note that the synthetic data extraction and adjoint sources injection are performed using  
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42 497 Kaiser-windowed sinc interpolation as well (Hicks, 2002).

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45 498 We use a North Sea exploration scale synthetic model in our testing. First we consider  
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47 499 a constant density noise-free experimental setup (inverse crime), for which we carry out  
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50 500 an in-depth analysis as well as a sensitivity study. Second, we design a more realistic  
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52 501 experimental setup using the same model.  
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## 502 **Inverse crime settings**

503 We first generate the observed data using the true model shown in Figure 13a. The finite  
504 differences grid points spacing is set to 25 m, the time step is 0.003 s and the total number  
505 of time steps is 4000. The source wavelet is a Ricker wavelet with 4 Hz central frequency, it  
506 is filtered with a high-pass filter with cutoff frequency of 2 Hz (Figure 14). The acquisition  
507 used for the tests in this section is a fixed-spread acquisition, with 128 sources, spaced with  
508 132 m, and 170 receivers spaced with 100 m. The starting model is obtained by a Gaussian  
509 smoothing of the true model (Figure 13b).

510 [Figure 13 about here.]

511 [Figure 14 about here.]

512 Before diving into a deeper analysis, we make a comparison of conventional FWI,  
513 extended-receiver FWI with static relocalization ( $\alpha = 0.375$ ) and our time-dependent ap-  
514 proach ( $\alpha = 0.01$ ,  $\beta = 0.25$ , with one segment and two control points). We perform 300  
515 iterations for all cases, the results are shown in Figure 15. As expected conventional FWI  
516 struggles to reconstruct the true velocity, from this crude starting model. Static receiver ex-  
517 tension provides a better reconstruction, however with visible defects. The time-dependent  
518 approach on the other hand, is able to better reconstruct the velocity model from this crude  
519 starting model. We show the model error as a function of FWI iterations in Figure 16. The  
520 model error is computed using

$$E = \frac{100}{M} \sum_i^M = \frac{|m_{est,i} - m_{true,i}|}{|m_{true,i}|}, \quad (35)$$

521 where  $M$  is the total number of model points,  $m_{est,i}$  is the estimated model at point  $i$  and  
 522  $m_{true,i}$  is the true model at point  $i$ . The model error for the conventional FWI increases at  
 523 first, then decreases to 9%, a value higher than the error at the starting model. Static receiver  
 524 extension performs better: the model error is mainly decreasing. The time-dependent ap-  
 525 proach provides the best reconstruction, the model error decreases quickly to a lower model  
 526 error.

527 To better understand why it works, we take a look at the data fit for both static and time-  
 528 dependent extension approaches (Figures 17 and 18). At the first iteration a better fit is  
 529 obtained using the time-dependent approach (blue and black on the Figures indicate a good  
 530 fit). As the model estimate improves, the relocalization tends to zero, this is apparent at the  
 531 last iteration. This can be better assessed by looking at the adjoint source (data residuals)  
 532 in Figure 19. The adjoint source at the last iteration of the time-dependent approach has the  
 533 lowest values, compared to the static approach, and the conventional FWI. This is indicative  
 534 of a better model reconstruction. Time-dependent receiver extension is able to reach a lower  
 535 model error, and a lower relocalization at the final iteration. This is not the case for the static  
 536 approach, where at the last iteration, the relocalization is still important. Better explaining  
 537 the data when the model estimate is poor, leads to a better model reconstruction.

538 [Figure 15 about here.]

539 [Figure 16 about here.]

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540 [Figure 17 about here.]  
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541 [Figure 18 about here.]  
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542 [Figure 19 about here.]  
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543 To complement our analysis, we show the misfit function evolution as a function of  
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544 FWI iterations, for the static and time-dependent cases in Figures 20a and 20b, respectively.  
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545 The data fit term ( $L_2$  norm of the data residuals without using relocalization) is shown as  
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23  
546 well (red line plot). The  $L_2$  misfit increases at first while the extended-receiver FWI is  
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547 decreasing, which indicates that  $L_2$  FWI would have been stuck in a local minimum. We  
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27  
548 note also the rapid reduction of the time-dependent approach cost function, as opposed  
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549 to the static counterpart. The  $L_2$  norm of the data residuals for the static relocalization  
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550 case increases at first (similar to the time-dependent approach), but then it stagnates after  
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551 a brief decrease, which indicates a slow convergence. Next, we take a look at the receiver  
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552 relocalization evolution as a function of outer-loop iterations. It is shown solely for the  
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553 leftmost, center and rightmost shot gathers. We obtain it using  
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$$R_1 = \frac{1}{N_r} \sum_{r=1}^{N_r} \sqrt{\int_0^T |\Delta x_r(t)|^2 dt}. \quad (36)$$

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554 The receiver relocalization can viewed as a proxy for model error, larger relocalization  
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555 indicates a poor model estimate. The relocalization decreases almost monotonically for  
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556 both approaches (Figure 21), however, the time-dependent approach reaches lower relocal-  
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557 ization, faster. For the time-dependent case we can also visualize the receiver speed as a

function of outer loop iterations, which is obtained using

$$R_2 = \frac{1}{N_r} \sum_{r=1}^{N_r} \sqrt{\int_0^T |\Delta \dot{x}_r(t)|^2 dt}. \quad (37)$$

The receiver speed decreases monotonically as the model estimates improves (Figure 22). The receiver speed is not too large (maximum of  $\approx 500 \text{ m.s}^{-1}$  for the leftmost and rightmost gathers), thanks to the second penalty term. This is an expected behavior, as the model estimate improves, there is less need for the receiver to move too fast.

For the tests we showed here, we set  $\alpha = 0.375$  for the static approach, and for the time-dependent approach we set  $\alpha = 0.01$  and  $\beta = 0.25$ . How would extended-receiver FWI behave when these tuning parameters are perturbed? We answer this question in the next paragraphs.

[Figure 20 about here.]

[Figure 21 about here.]

[Figure 22 about here.]

## Sensitivity to the tuning parameters

In this section we investigate how the tuning parameters in our cost function ( $\alpha$  and  $\beta$ ) impact the model reconstruction, the data fit and the convergence. We carry out three sets of tests: [1]  $\alpha$  variations impact on static receiver extension, [2]  $\alpha$  variations impact

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4 574 on time-dependent receiver extension for a constant value of  $\beta$ , and [3]  $\alpha$  and  $\beta$  variation  
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7 575 impact on the time-dependent receiver extension. We keep the same experimental setup  
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9 576 (Figure 13). For each experiment 300 outer loop iterations are performed. For the inner  
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11 577 loop, we use one segment with first order Lagrange polynomial giving a two degrees of  
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14 578 freedom problem, which we solve with a grid-search. We do this in order to avoid the PSO  
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16 579 tuning parameters impacting our sensitivity testing.  
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21 580 *Static receiver extension: sensitivity to  $\alpha$*   
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25 581 For this first set of experiments we test 24 equally spaced values of  $\alpha \in ]0, 1]$ . Extended-  
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27 582 receiver FWI is then carried out using static relocalization. We show the cost function at the  
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29 583 last iteration as well as the model error as function of  $\alpha$  in Figure 23a and 23b, respectively.  
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31  
32 584 The cost function at the last iteration increases –in the most part– with increasing  $\alpha$  with  
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34 585 a few outliers. The first outlier corresponds to  $\alpha = 0.125$ , it is caused by a line-search  
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36 586 failure (that is, the line-search process in the outer loop was unable to find an adequate step  
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38 587 length). The second outlier corresponds to the lowest cost value that was achieved with  
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41 588  $\alpha = 0.375$ . Two other points,  $\alpha = 0.333$  and  $\alpha = 0.416$  do not follow the trend as well.  
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44 589 These four points and two others, namely,  $\alpha = 0.583$  and  $\alpha = 0.791$  are shown as black  
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46 590 circles in Figures 23a and 23b. The corresponding models are shown in Figure 24, this is  
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48 591 discussed in the next paragraph. Increased cost at the last iteration with increasing  $\alpha$  is -in  
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51 592 theory- expected, as the relocalization is constrained more with increasing  $\alpha$ . However,  
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53 593 we note that the static relocalization is sensitive to small variation in the tuning parameter.  
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56 594 As for the model error, it varies with  $\alpha$ , but the variation is less apparent. We also note  
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4 595 that the model error is high for all  $\alpha$  values, which indicates that the model reconstructions  
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6 596 are not satisfactory. The relocalization at the first and last iterations (Figures 23c and 23d,  
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8  
9 597 respectively) are as expected, the values decrease with increasing  $\alpha$  values. It is interesting  
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11 598 to note that the relocalization value at the last iteration, for small  $\alpha$  values is high. This  
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13 599 means that the model reconstruction is not satisfactory, otherwise, the relocalization would  
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16 600 tend to zero.

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19 601 We show the reconstructed models that correspond to the selected  $\alpha$  values in Figure 24.  
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21 602 The selected  $\alpha$  values are shown as circles in Figures 23a 23b. This approach appears to be  
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23 603 sensitive to the choice of  $\alpha$ . Small variations of the tuning parameter, lead to a significant  
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25 604 change in the reconstructed model. This means that the static relocalization approach is  
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28 605 difficult to tune.

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33 606 [Figure 23 about here.]

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37 607 [Figure 24 about here.]

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41 608 *Time-dependent relocalization: sensitivity to  $\alpha$*

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45 609 We perform a similar numerical experiment using our time-dependent strategy, we set  
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47 610  $\beta = 0.25$  and we test the 24  $\alpha \in ]0, 1]$ . The results are shown in Figure 25. The choice of  
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49 611  $\alpha$  appears to have less impact on the cost function at the last iteration, and lower values are  
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51 612 reached, this is not the case for the static approach. Note that we use the same normalization  
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53 613 to obtain the normalized cost, for the static and the time-dependent approaches, this is  
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55 614 done in order to keep the cost function plots comparable. The tuning parameter does not  
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5 615 have a significant impact on the model error, we note also that a lower model error is  
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7 616 reached for all  $\alpha$  values, compared to the static counterpart. The impact of this tuning  
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9 617 parameter on the relocalization at the first iteration appears to be –roughly– linear, the  
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11 618 relocalization decreases with increasing  $\alpha$ , which is an expected behavior. As for the last  
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14 619 iteration,  $\alpha$  appears to have no observable effect, and the relocalization tends to zero. This  
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16 620 is an indication of good model reconstruction. Our approach appears to be less sensitive  
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18 621 to the choice of the tuning parameter  $\alpha$ . We show the reconstructed models (Figure 26)  
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21 622 corresponding to the same selected  $\alpha$  values for the static case. These values are indicated  
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23 623 by black labeled circles in Figure 25a and 25b. The effect of  $\alpha$  on the reconstruction appears  
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25  
26 624 to be minimal. This is an encouraging observation, as it means that the method is easy to  
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28 625 tune. For these tests, the  $\beta$  value has been kept constant, how does our method behave  
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31 626 when both  $\alpha$  and  $\beta$  are perturbed? To answer this question, we devise a parametric study  
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33 627 which we discuss in the next paragraphs.

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37 628 [Figure 25 about here.]

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41 629 [Figure 26 about here.]

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46 630 *Time-dependent relocalization: sensitivity to  $\alpha$  and  $\beta$*

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50 631 In order to understand how the two tuning parameters  $\alpha$  and  $\beta$  impact our strategy, we  
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52 632 conduct a parametric study scanning for a different  $\alpha$  and  $\beta$  values. This is a computation-  
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54 633 ally expensive test, therefore, we use a non-regular grid. The tuning parameters values are  
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57 634 shown in Table 1, where the first row shows the  $\alpha$  and  $\beta$  values we consider, and the second

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4 635 row shows the additional values that are considered only for the  $\beta$  parameter.  
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8 636 [Table 1 about here.]  
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12 637 Following the same setup as before, we run extended-receiver FWI for 300 iterations  
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14 638 for each combination of  $\alpha$  and  $\beta$ . We show the result in Figure 27 using a logarithmic scale  
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16 639 for both axes. Similar to the previous test, the time-dependent strategy appear to be less  
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18 640 sensitive to the choice of  $\alpha$ . This can be seen in the cost obtained at the last iteration, and  
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20 641 also in the model error, shown in Figures 27a and 27a, respectively. The minimum cost  
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22 642 is obtained for  $\alpha = 0.025$  and  $\beta = 0.25$ , and the minimum model error for  $\alpha = 0.0075$   
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24 643 and  $\beta = 0.75$ . We show the corresponding final models in Figures 28a and 28b. The  
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26 644 reconstructed models are mostly good, regardless of the choice of the tuning parameters.  
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28 645 However, for large  $\beta$  values, the model reconstruction is impacted, which can be seen on  
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30 646 the relocalization (leftmost and rightmost shot points). This occurs when  $\beta$  is large: the  
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32 647 method then behaves as static relocalization, the receiver speed being heavily constrained.  
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34 648 The best results are obtained for reasonably low  $\beta$  values (not greater than 0.75 based on  
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36 649 our findings from this experiment). This test concludes the investigations done in inverse  
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38 650 crime settings. Next, we design a more realistic experimental setup.  
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48 651 [Figure 27 about here.]  
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52 652 [Figure 28 about here.]  
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## 653 **Realistic settings**

654 We now use the same North Sea exploration scale 2D synthetic model in a more realistic  
655 setting. First, the observed data are computed under the visco-acoustic approximation using  
656 the  $V_p$ ,  $\rho$  and  $Q_p$  models, shown in Figure 29. The source wavelet is a Ricker centered at 4  
657 Hz. It is filtered with a high-pass filter with cutoff frequency of 2 Hz. As for the acquisition,  
658 it is a fixed-spread setup, with 128 sources spaced with 117.5 m, and 150 receivers spaced  
659 with 100 m. The discretization step used for the finite differences is set to 12.5 meters,  
660 the time step is set to 0.0015 seconds, and the number of time steps is 6000. The data  
661 are decimated to a time step of 0.003 seconds, and a band-limited Gaussian noise is added  
662 (Figure 30). The discretization step used for the forward computations during the inversion  
663 is set to 25 meters. For the receiver extension, we set  $\alpha = 0.01$  for both the static and  
664 time-dependent cases. Only for the time-dependent approach, we set  $\beta = 0.0025$ , and the  
665 time-dependent relocalization is parametrized with one segment and two control points.

666 [Figure 29 about here.]

667 [Figure 30 about here.]

668 The starting velocity model is a 1D model (obtained with  $V_p^{1D}(z) = 0.38z + V_p^{water}$ ),  
669 the starting density model is obtained using Gardner's law on the starting velocity model,  
670 which is given by  $\rho(x) = 1740(10^{-3}V(x))^{\frac{1}{4}}$ . The quality factor is set to 100 everywhere,  
671 except in the water layer where it is set to 1000. The starting models are shown in Figure  
672 31. For these numerical tests we only update the velocity during the inversion. First we

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4 673 perform a source time function estimation in the starting velocity model (Pratt, 1999), the  
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6 674 result of which is shown in Figure 32. The inversion is performed for 300 iterations using  
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9 675 conventional FWI, static receiver extension, and time-dependent receiver extension, with  
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11 676 the previously computed wavelet.  
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15 677 [Figure 31 about here.]  
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19 678 [Figure 32 about here.]  
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23 679 We show the reconstructed models after the 15, 110, 205 and 300 iterations in Fig-  
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25 680 ure 33. As expected, conventional FWI is unable to reconstruct the velocity from the 1D  
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28 681 starting model. Static relocalization performed a bit better, however, some high velocity  
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30 682 artifacts are present in the low velocity anomaly in the center of the model. The time-  
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32 683 dependent approach provides the best model reconstruction. The low velocity anomaly is  
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34 684 fully reconstructed, as well as most of the higher velocity basement. We show the data fit  
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37 685 as well as the relocalization gathers, for the first and last iterations for both approaches in  
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40 686 Figures 34 and 35. A good fit is obtained at the first iteration for both strategies. However,  
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42 687 at the last iteration the data fit prior to relocalization is better for the time-dependent case.  
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44 688 Moreover, the receiver relocalization is lower at the last iteration for the time-dependent  
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47 689 case, which indicates a better model reconstruction. These results in a 2D realistic setting  
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49 690 are very encouraging.  
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53 691 [Figure 33 about here.]  
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57 692 [Figure 34 about here.]  
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[Figure 35 about here.]

## DISCUSSION

In this section we discuss the following points: [1] the use of the second penalty term ( $\mathcal{P}_2$  in equation 19) and the Doppler effect, [2] the choice of PSO as our global optimization scheme, and [3] finally the computational overhead of our strategy with respect to more conventional FWI approaches.

### The term $\mathcal{P}_2$ and the Doppler effect

The second penalty term is added to constrain the receiver speed. This is important as moving receivers, or moving sources alter the frequency content of the data. In our case, we encounter both situations. The calculated data extraction from the wavefield at a moving receiver positions, with a stationary source, causes a change in the frequency content. A moving source is encountered during the adjoint simulation, where the adjoint source (our receiver), is moving as a function of time, which in turn, can cause the frequency content change. These frequency content changes are attributed to the Doppler effect. For the moving receiver case, these effects can be better understood by looking at the Doppler effect formula

$$f = \frac{v_p \pm v_r}{v_p} f_o, \quad (38)$$

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4 708 where  $f$  is the observed frequency, and  $f_o$  is the emitted frequency.  $v_p$  is the medium  
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6 709 velocity and  $v_r$  is the receiver speed. The latter is added if the receiver is moving towards  
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9 710 the source, and subtracted in the other case. Equation (38) is for the case where the source is  
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11 711 stationary and the receiver is moving. If the source is moving and the receiver is stationary  
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14 712 (the adjoint simulation), the observed frequency is given by

$$f = \frac{v_p}{v_p \pm v_s} f_o, \quad (39)$$

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23 713 where  $v_s$  is the source speed, it is added if the source is moving away from the source,  
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25 714 and it is subtracted in the other case. We illustrate the moving receiver case in Figure 36,  
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27 715 using the same 2 layers setup shown in Figure 4. The spectrum of the calculated data,  
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29 716 which is extracted at the time-dependent receiver position without using the second penalty  
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31 717 term ( $\beta = 0$ ) is shown in red. The blue curve is obtained with  $\beta = 0.001$ , and the green  
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34 718 curve is for the static relocation case (the receiver position does not depend on time).  
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37 719 In the case where no constraint is imposed on the receiver speed (red plot) we can see that  
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39 720 the spectrum is different. In particular, energy at low frequencies is added, this is due to  
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42 721 Doppler effect for a receiver moving away from the source. When the receiver speed is  
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44 722 constrained ( $\beta = 0.001$ ), the spectrum is much closer to the one obtained with  $\beta = \infty$ ,  
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47 723 therefore mitigating the Doppler effect.

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51 724 [Figure 36 about here.]  
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55 725 Another interesting observation can be made for the experiment where the source is  
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57 726 moving (an adjoint source, our receiver). We show the adjoint field at time 3.18 s in Figure  
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4 727 37a. The source is moving to the right at a speed which is higher than the medium velocity,  
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7 728 the structure that appears on the left of the moving source is called a Mach cone. The  
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9 729 gradient resulting from this adjoint field is shown in Figure 37b, the positions occupied by  
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11 730 the moving receiver are superimposed to the gradient, the color map indicates the receiver  
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14 731 speed. Numerical artifacts are present in our gradient, which are caused by the frequency  
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16 732 increase, which in turn, stems from the Doppler effect.

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20 733 [Figure 37 about here.]

## 21 22 23 24 734 **Choice of a global optimizer**

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28 735 In a previous work (Benziane et al., 2023), we have investigated various methods for the  
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31 736 solution of the inner loop problem. Namely, Markov-chain Monte Carlo methods (Aster  
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33 737 et al., 2013), simulated annealing (Sen and Stoffa, 2013), and a variation of it, Very Fast  
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35 738 Simulated Annealing or VFSA (Ingber, 1992, 1993). McMC is in fact a very good method  
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38 739 for exploring the parameter space, and inferring the posterior distribution. The sought dis-  
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40 740 tribution (the posterior) is inferred by randomly sampling a proposal distribution. Each  
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43 741 sample is either accepted or rejected using the Metropolis-Hastings criterion (Metropolis  
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45 742 et al., 1953; Hastings, 1970). However, it is very costly, because many misfit evaluations  
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48 743 are required for the Markov-chain to converge to a stationary distribution. Simulated an-  
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50 744 nealing is similar to McMC, as it also uses a Markov-chain, however, the probability of  
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52 745 accepting a candidate solution is decreased along the iterations, making use of the so-  
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55 746 called "cooling schedules". The cooling schedule forces the acceptance probability to be  
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57 747 large for most candidate solutions at earlier iterations, which translates to a high acceptance  
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4 748 rate. This probability is reduced using the cooling schedule, which could drastically reduce  
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7 749 the acceptance rate. Simulated annealing is not very well adapted to our problem, as it  
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9 750 suffers from premature convergence. This premature convergence to a local minimum oc-  
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11 751 curs when the best candidate reached by the Markov-chain is a local minimizer, while the  
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14 752 probability of acceptance decreases, making this local minimizer overwhelmingly proba-  
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16 753 ble. Furthermore, it was notoriously difficult to tune, namely, choosing a cooling schedule  
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18 754 and its parameters. Very Fast Simulated Annealing suffers from convergence issues for our  
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21 755 problem, although, it is easier to tune than conventional simulated annealing, as it relies on  
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23 756 a single cooling schedule and a single generating distribution, which reduces the number of  
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26 757 tuning parameters. Grid-search is of course costly, even for the simplest parametrization we  
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28 758 can consider (one segment with first order Lagrange polynomial, giving a two dimensional  
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31 759 problem).

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34 760 In order to illustrate this, we use a North Sea Exploration Scale synthetic model. We  
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36 761 keep the same setup, which is shown in Figure 9. We consider two segments with first order  
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38 762 Lagrange polynomials, giving a three degrees of freedom problem. We compare different  
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41 763 global optimization schemes, namely, McMC, VFSA and PSO. First, we sample the inner  
42  
43 764 loop misfit function using McMC (Figure 38). This plot is obtained by cross-plotting each  
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46 765 dimension against another, couple by couple. In other words, for a given point sampled by  
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48 766 McMC in this 3-D space, with the coordinates  $(a_1, a_2, a_3)$ , we plot its position in 2-D as  
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51 767 such,  $a_1$  is plotted against  $a_2$  and then against  $a_3$ . We assign the value of the cost function  
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53 768 to the sample providing the color map shown. The diagonal shows the histogram in each  
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56 769 dimension. Thanks to the McMC sampling, we can see the inner loop misfit function,

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4 770 which contains many local minima. The misfit function corresponding to the couples  $a_3/a_1$ ,  
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6 771 and  $a_2/a_3$ , varies slowly compared to the other couples, and the histograms for  $a_3$  is flat.  
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9 772 This is expected, as the point points  $a_1$  and  $a_3$  correspond to the start and the end of the  
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11 773 seismic trace, respectively. The data values at early times, as well as very late time (time  
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13 774 steps closer to the end of the trace) are close to zero. This reduces the sensitivity to  $a_1$  and  
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16 775  $a_3$ , this is particularly true for  $a_3$ .

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19 776 We carry out the inner-loop optimization using McMC, VFSA and PSO. We show the  
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21 777 evolution of the cost as a function of iterations in Figure 39. Note that the McMC plot shows  
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23 778 only samples that reduce the cost function, otherwise, the plot would be cluttered. For this  
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25 779 McMC example, a total of  $2.5 \times 10^6$  misfit evaluations have been performed. But the plots  
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27 780 show only 25000 samples, as we did a burn-in period of 5000 iterations and a skipping  
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29 781 step of 500 iterations. This is done to avoid the correlation effects between samples, which  
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31 782 stem from the pseudo-random number generation process (Aster et al., 2013). McMC did  
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33 783 in fact provide a good solution, but it required a large number of cost function evaluations.  
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35 784 VFSA did not converge to a meaningful solution, which is clear in the cost function plot.  
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37 785 PSO gave the most interesting result, converging quickly to the global minimum. This  
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39 786 population based strategy is well adapted to our problem, this can be seen in Figure 39b.  
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41 787 The personal best cost for few particles are shown, different particles explore in the vicinity  
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43 788 of various minima, leading to a convergent behavior of the swarm. That is why we use PSO  
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45 789 for the inner loop optimization. Furthermore, PSO tuning was less challenging thanks to  
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47 790 the few published meta-optimization studies (Pedersen, 2010; Mason et al., 2018), where  
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49 791 we obtained the PSO parameters.  
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792 [Figure 38 about here.]

793 [Figure 39 about here.]

## 794 Computational cost

795 The CPU times we show in Table 2 correspond to the realistic setting example we  
796 showed earlier (Figure 29). Please note that we use Checkpointing Assisted Reverse For-  
797 ward Simulation (CARFS) for the gradient computation (Yang et al., 2016a) for all our  
798 numerical experiments. We have a slight increase in the forward computation CPU time  
799 for both static and time-dependent receiver extension, this is caused by the decimation and  
800 storage of a portion of the wavefield that we use for the extension. The main computation  
801 overhead comes from the inner loop optimization. The computational burden for the static  
802 receiver extension is minor. However, for the time-dependent approach the inner loop com-  
803 putation is more important. An increase in the gradient computation CPU time is caused  
804 by the adjoint-source injection. We recall the adjoint equation

$$\begin{cases} A(m)^T \lambda_s[m, \overline{\Delta x(t)}](\mathbf{x}, t) = \sum_{r=1}^{N_r} \tilde{R}_{s,r}^T[\overline{\Delta x_r(t)}] \tilde{\mu}_s[m](\mathbf{x}_r + \overline{\Delta x_r(t)}, t), \\ \tilde{\mu}_s[m](\mathbf{x}_r + \overline{\Delta x_r(t)}, t) = \tilde{d}_{cal,s}[m](\mathbf{x}_r + \overline{\Delta x_r(t)}, t) - d_{obs,s}(\mathbf{x}_r, t). \end{cases} \quad (40)$$

805 The cost of adjoint simulation is more important for the time-dependent approach, as  
806 we use Kaiser windowed sinc interpolation (Hicks, 2002) to inject the adjoint the sources  
807 at moving receivers positions. This is performed for all receivers at every time step. Even  
808 though the cost increase is not negligible, it is certainly manageable. Also, the convergence

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4 809 to a good model is obtained faster.  
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7 810 To put the computation overhead into perspective, we take a look at the time complexi-  
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9 811 ties. The time complexity for the forward and adjoint simulations is  $\mathcal{O}(n^2)$  in 2D and  $\mathcal{O}(n^3)$   
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12 812 in 3D. As for the inner-loop, the complexity in term of the number of receivers is  $\mathcal{O}(n)$  in  
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14 813 2D, and  $\mathcal{O}(n^2)$  in 3D. The large number of receivers in 3D can constitute a bottleneck. We  
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17 814 address this point in the conclusion of this paper.  
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21 815 [Table 2 about here.]  
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## 26 CONCLUSION AND PERSPECTIVES

### 27 28 29 30 816 **Conclusion** 31 32 33

34 817 Extended-receiver FWI with time-dependent relocalization have shown promising re-  
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36 818 sults. The ease with which this method is directly applied to time-domain FWI, as well  
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39 819 as the simplicity of tuning its misfit function are very encouraging. Another advantage is  
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41 820 that there is no need to adjust the tuning parameters during the inversion. The speed of  
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44 821 convergence from very crude starting models is another attractive feature. However, the  
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46 822 method comes with a non-negligible but certainly manageable computation cost.  
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### 51 823 **Perspectives and ongoing work** 52 53 54

55 824 The next step of our work is extending the method to 3D as well as an application to a  
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57 825 field dataset. The 3D extension of this method relies on the idea of allowing the receivers to  
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4 826 move either towards or away from the source, following a fixed angle defined by the source  
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7 827 and receiver positions. The preliminary results in 3D synthetic settings are encouraging.  
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10 828 The 3D implementation comes with a caveat: the increasing the number of receivers.  
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12 829 This has encouraged us to develop an alternative parametrization and optimization for the  
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14 830 inner-loop, in order to make the cost manageable for 3D application. This strategy relies on  
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17 831 the observation that the receiver relocalization problem broken down into a series of nested  
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19 832 smaller problems, in a similar fashion to dynamic time warping (Hale, 2013), which can be  
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22 833 solved deterministically. This approach is considerably less costly than the stochastic ap-  
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24 834 proach described herein. Testing in 3D settings using our dynamic programming approach  
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27 835 is ongoing.  
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## APPENDIX A

### FULL MISFIT FUNCTION EXPRESSION FOR EXTENDED-RECEIVER FWI

836 We write the full expression of the receiver-extension misfit function

$$\begin{aligned}
 \min_{m, \Delta x} \tilde{f}(m, \Delta x) = \min_{m, \Delta x} & \frac{1}{2} \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \int_0^T |\tilde{d}_{cal,s}[m](\mathbf{x}_r + \Delta x_r, t) - d_{obs,s}(\mathbf{x}_r, t)|^2 dt \\
 & + \frac{\alpha}{2} \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \|d_{obs,s,r}\|_{\infty}^2 \frac{\|\Delta x_{s,r}\|_2^2}{L^2}.
 \end{aligned} \tag{A-1}$$

837 the second term in the right hand side is the penalty term ( $\mathcal{P}_1$  in equation 8), it prevents  
 838 the relocalization from being too large, and forces the receiver to its original position as  
 839 the model estimate improves. In this penalty term,  $L$  is the maximum allowed receiver  
 840 relocalization, and  $\alpha$  is a tuning parameter.

841 Similarly, we write the misfit function of the extended-receiver FWI with time-dependent  
 842 relocalization

$$\begin{aligned}
 \min_{m, \Delta x} \tilde{f}(m, \Delta x) = \min_{m, \Delta x(t)} & \frac{1}{2} \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \int_0^T |\tilde{d}_{cal,s}[m](\mathbf{x}_r + \Delta x_r(t), t) - d_{obs,s}(\mathbf{x}_r, t)|^2 dt \\
 & + \frac{\alpha}{2} \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \|d_{obs,s,r}\|_2^2 \frac{\|\Delta x_{s,r}\|_2^2}{L^2} \\
 & + \frac{\beta}{2} \sum_{s=1}^{N_s} \sum_{r=1}^{N_r} \|d_{obs,s,r}\|_2^2 \frac{\|\Delta \dot{x}_{s,r}\|_2^2}{V_{max}^2}
 \end{aligned} \tag{A-2}$$

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4 843 the second term in the right hand side of equation A-2 ( $\mathcal{P}_1$  in equation 19) penalizes the  
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7 844 receiver relocalization, in order to prevent it from being too large, and to force it to become  
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9 845 small along iterations.  $L$  is the maximum allowed receiver relocalization, and  $\alpha$  is a tuning  
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11 846 parameter, for weighting this penalty term. Similarly, the third term in the right hand side  
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14 847 of equation A-2 ( $\mathcal{P}_2$  in equation 19) penalizes the receiver speed (the first order derivative  
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16 848 with respect to time of the receiver relocalization).  $V_{max}$  is the maximum allowed receiver  
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19 849 speed, and  $\beta$  is a tuning parameter.  
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1049 10 Inner-loop illustration, (a): misfit function map, using one segment and  
1050 two control points, the global minimum is shown as a red star. (b): A cross  
1051 section following the black line in (a). Note how close are the values of the  
1052 global minimum (red vertical dashed line), and the secondary minimum  
1053 (blue vertical dashed line). (c): the observed shown in a black dashed line,  
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1072 the static case. We display the calculated data in a red and blue color scale  
1073 while the observed data is shown in gray-scale. If solely blue and black are  
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1077 the shot gather. The first iteration is shown in the first row(a,b,c), and the  
1078 last iteration is shown in the second (d,e,f). . . . . 80

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1085 the shot gather. The first iteration is shown in the first row(a,b,c), and the  
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1166 37 Gradient computation with  $\beta = 0$ . (a): adjoint field snapshot at 3.18 s, the  
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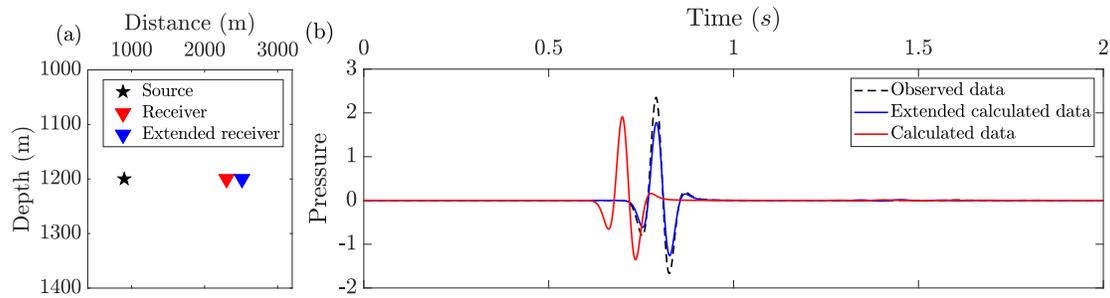


Figure 1: Receiver extension illustration. (a) Acquisition setup, the source is shown as a black star, the receiver position as a red triangle, and the extended receiver in blue, (b) observed trace (black dashed line), calculated trace (red solid line), and calculated trace extracted at the extended receiver position (blue solid line).

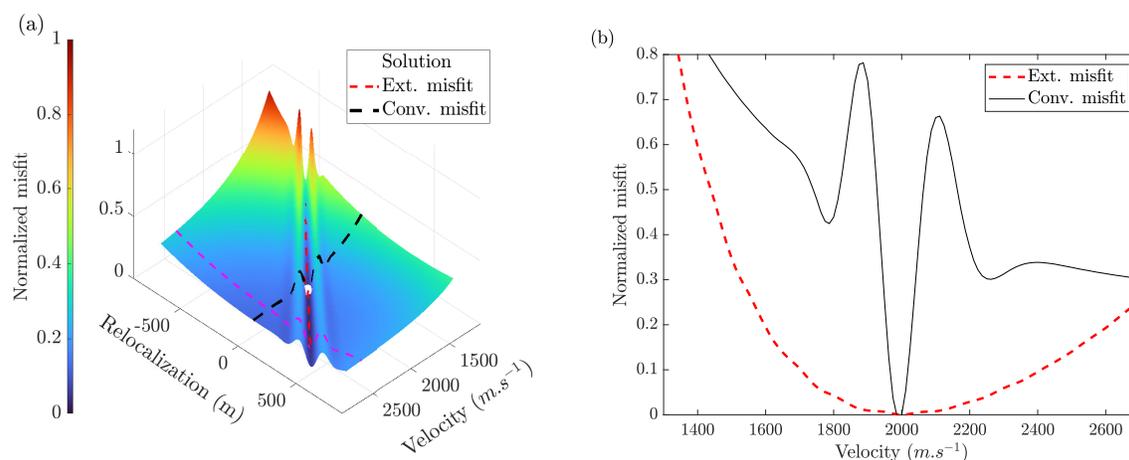


Figure 2: Illustration of the receiver-extension misfit function. (a) Misfit function 2D view as a function of velocity and receiver relocalization. The minimum is shown in white, the misfit values corresponding to the receiver-extension are shown in a red dashed line. The dashed magenta line indicates the velocity value at which the calculated data in Figure 1 are computed. (b) Misfit function profile along the zero-relocalization (conventional  $L_2$  misfit) in a solid black line, misfit function profile along the minimum value over the receiver relocalization  $\Delta x_{s,r}$  in a dashed red line.

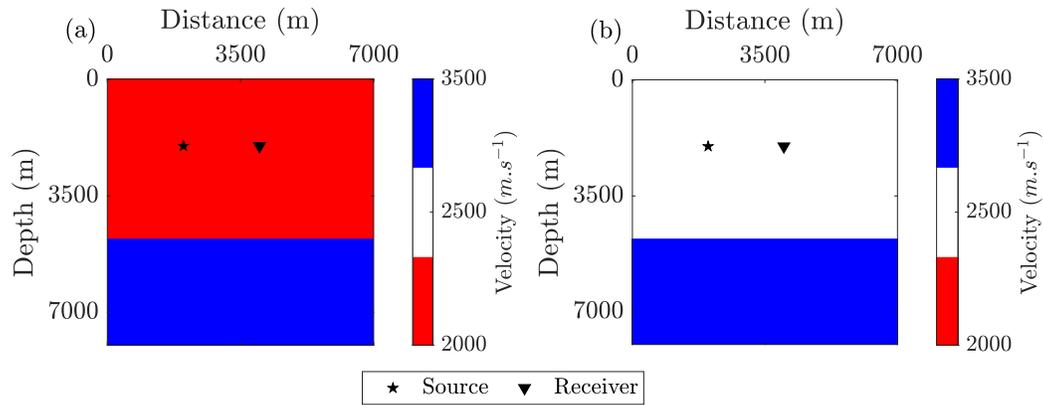


Figure 3: Experimental setup (a): true velocity model, (b): the starting model used for gradient illustration hereafter.

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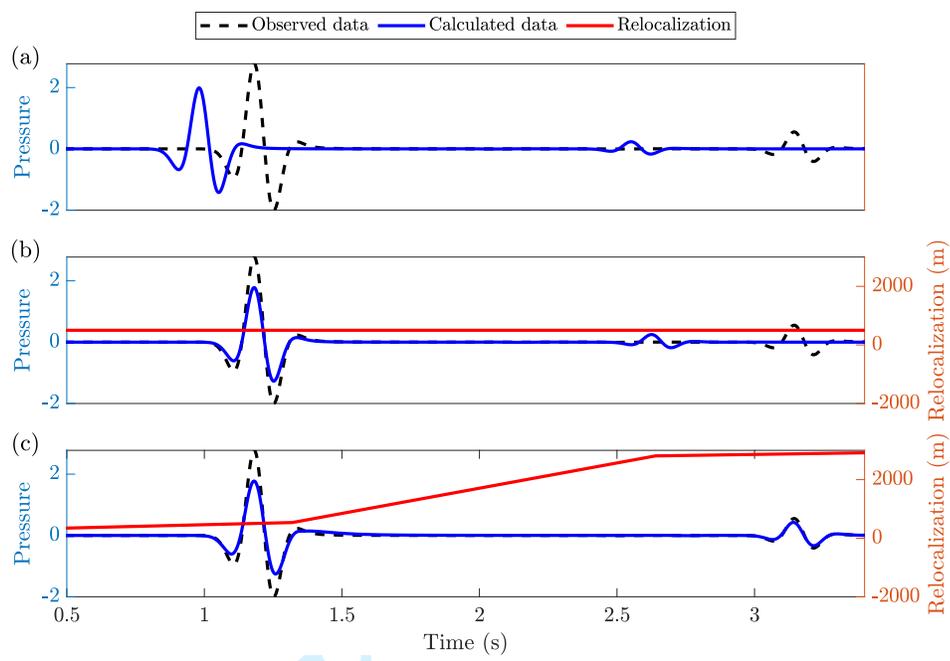


Figure 4: Observed and calculated data, as well as relocalization time profiles for: (a) conventional FWI, (b): static relocalization and (c): time-dependent relocalization.

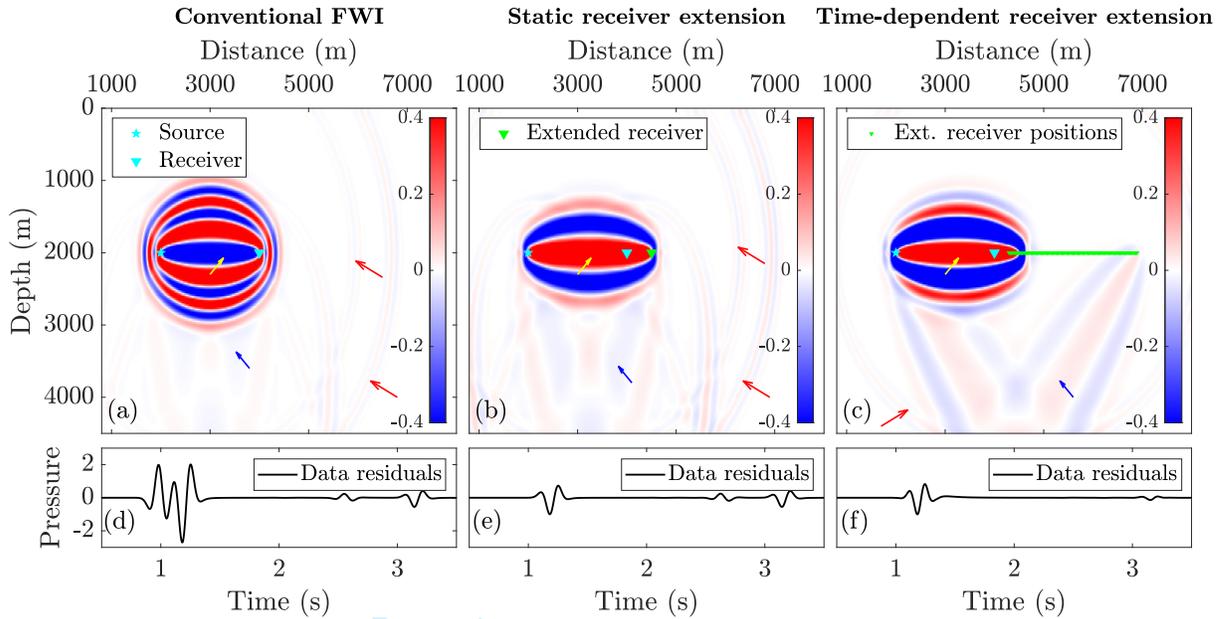


Figure 5: FWI kernels and adjoint sources for (a,d): conventional FWI, (b,e): static re-localization and (c,f): time-dependent re-localization. The yellow arrow indicates the first Fresnel zone, the blue indicates the rabbit-ears and the red arrows show the migration isochrones.

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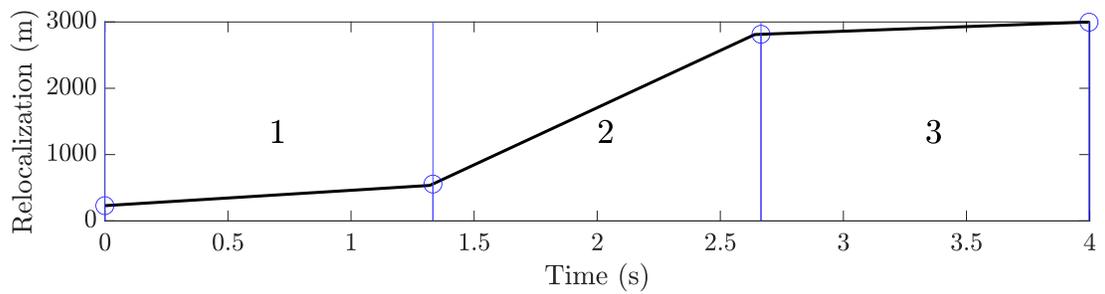


Figure 6: Time-dependent parametrization example, using three segments with first order Lagrange polynomials. The circles indicate the control points  $a_i$ .

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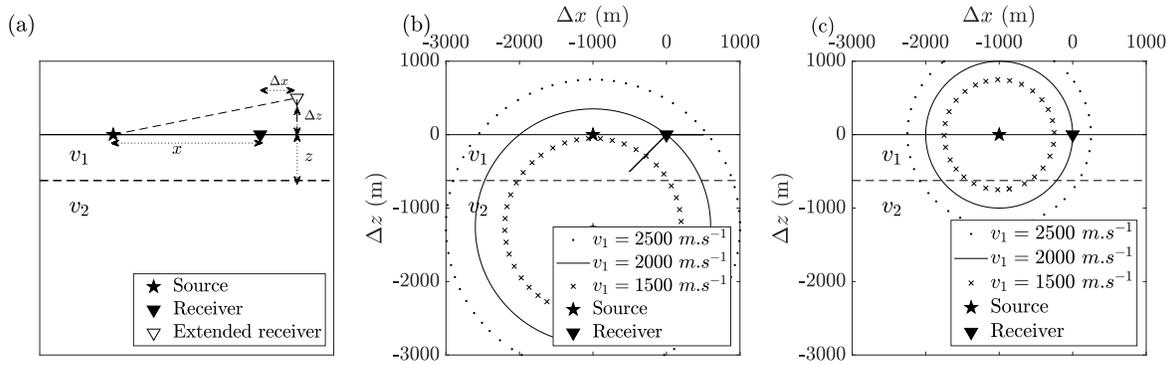


Figure 7: Simple reflection case analysis with receiver extension. The geometry is shown in (a), the original and extended receiver positions shown as a black, and white inverted triangles, respectively.  $\Delta x$  and  $\Delta z$  are the horizontal and vertical receiver relocalizations. The possible receiver relocalizations at different velocities for the reflection and transmission cases are shown in (b) and (c), respectively.

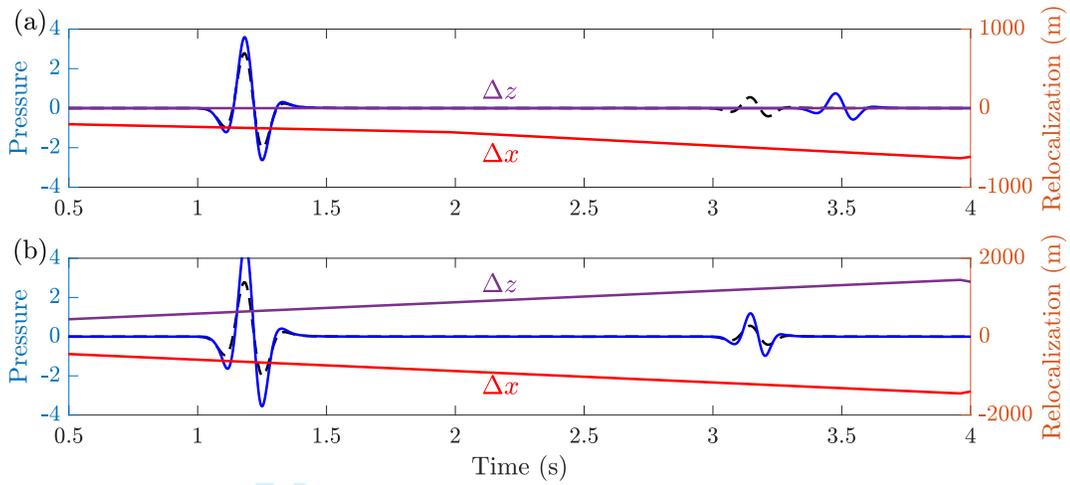


Figure 8: Data fit and relocalization profiles for a two arrivals case using a lower top layer starting velocity. (a): Time-dependent horizontal relocalization, and (b): time-dependent relocalization with both vertical and horizontal components. The observed trace is shown in a black dashed line, the calculated is shown in a blue solid line, the horizontal relocalization is shown in a red solid line, and the vertical in a purple solid line.

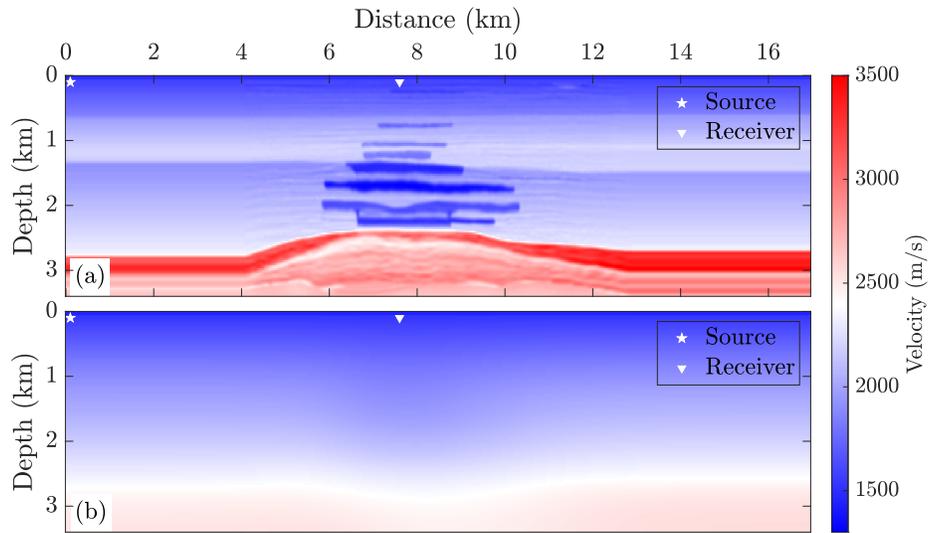


Figure 9: A North Sea exploration scale synthetic model, (a): true model, (b): starting model obtained by Gaussian smoothing of the true model.

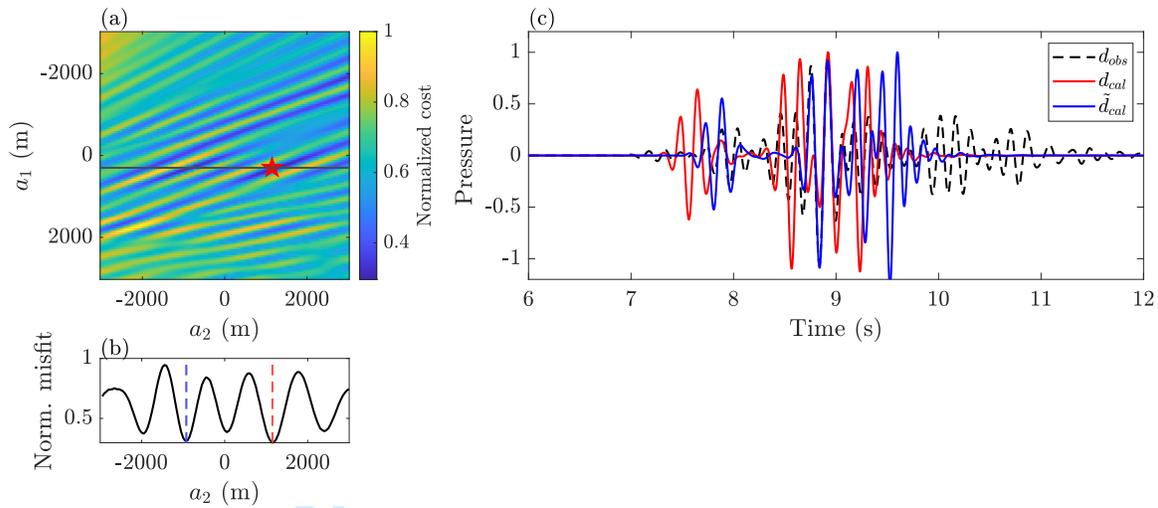


Figure 10: Inner-loop illustration, (a): misfit function map, using one segment and two control points, the global minimum is shown as a red star. (b): A cross section following the black line in (a). Note how close are the values of the global minimum (red vertical dashed line), and the secondary minimum (blue vertical dashed line). (c): the observed shown in a black dashed line, calculated in a red solid line and the extended data corresponding to the global minimum shown in a blue solid line.

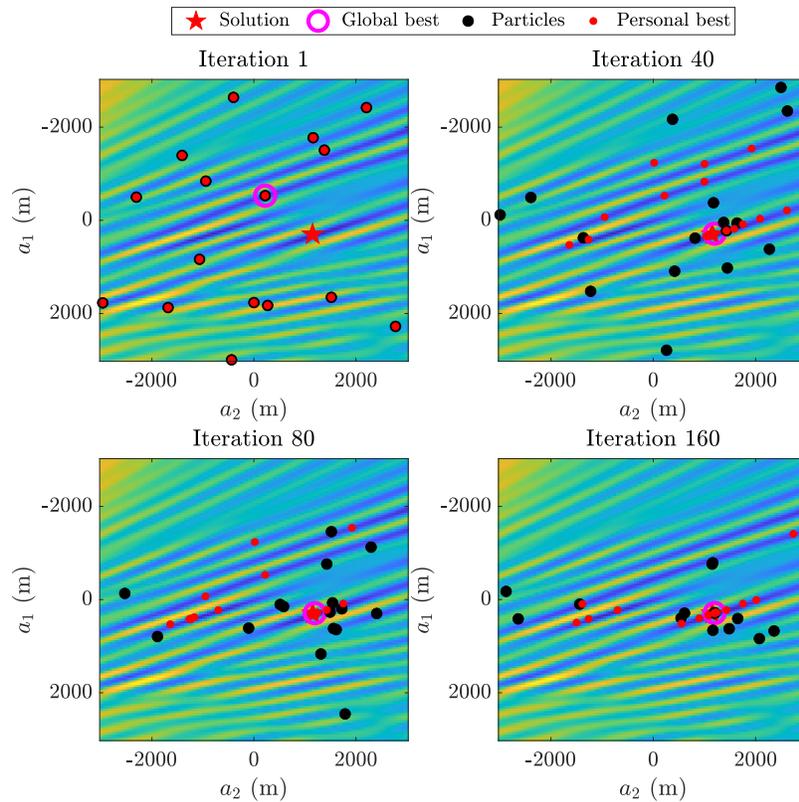


Figure 11: PSO example showing the swarm configuration at different iterations superimposed on the misfit map, the personal best positions are shown in cyan and the global best in magenta, the global solution (obtained with grid-search) is shown as a red star.

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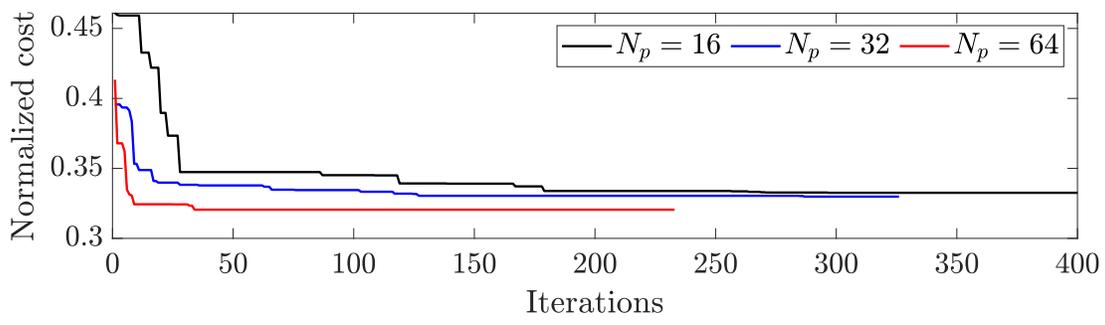


Figure 12: Global best normalized cost as a function of the number of iterations using 16, 32 and 64 particles.

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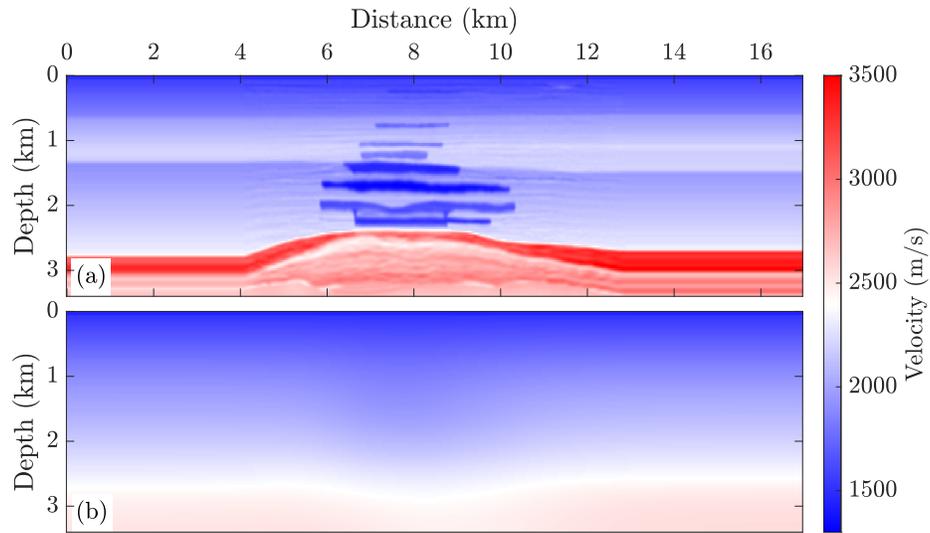


Figure 13: A North Sea exploration scale synthetic model. (a): true model used to generate the observed data, (b): the starting model.

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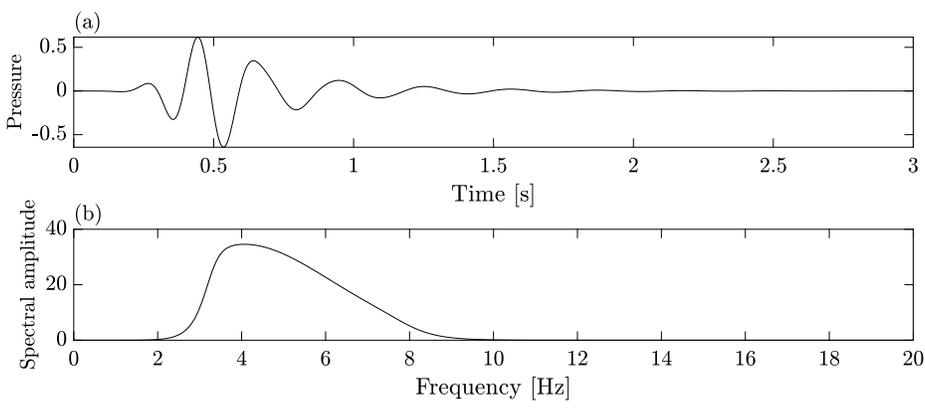


Figure 14: The source wavelet used for the numerical experiment. (a): time-domain (b): frequency domain.

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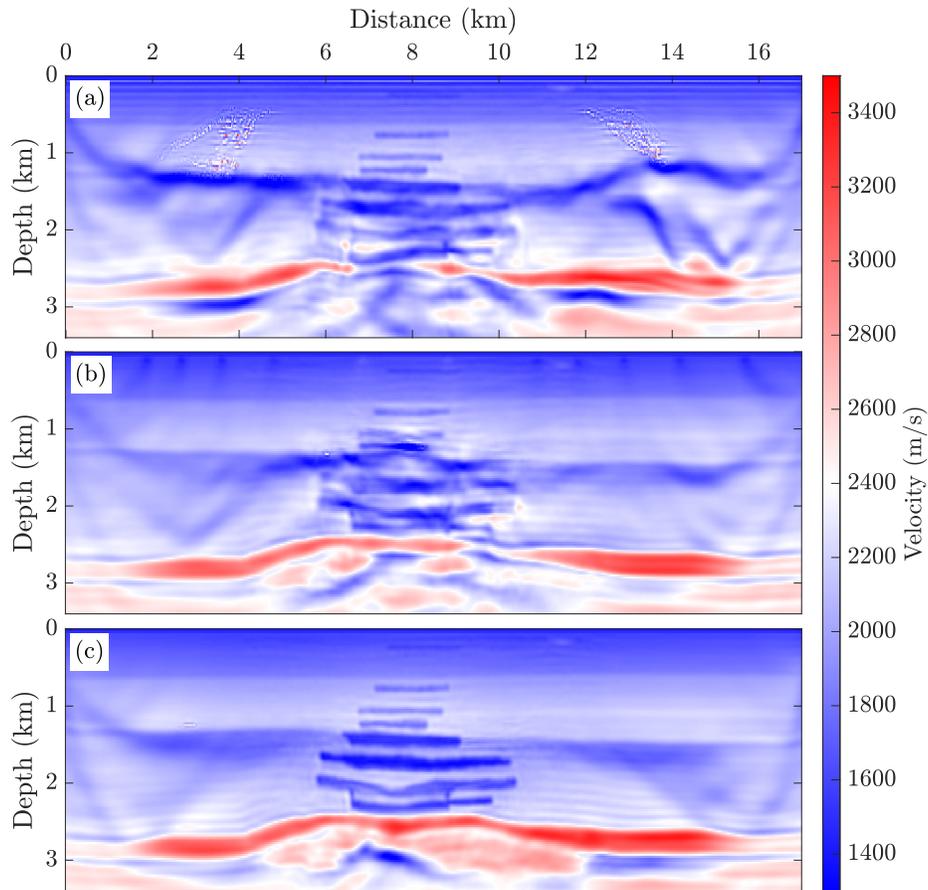


Figure 15: Reconstructed velocity models after 300 iterations. (a): conventional FWI, (b): static extended-receiver FWI and (c): time-dependent extended-receiver FWI.

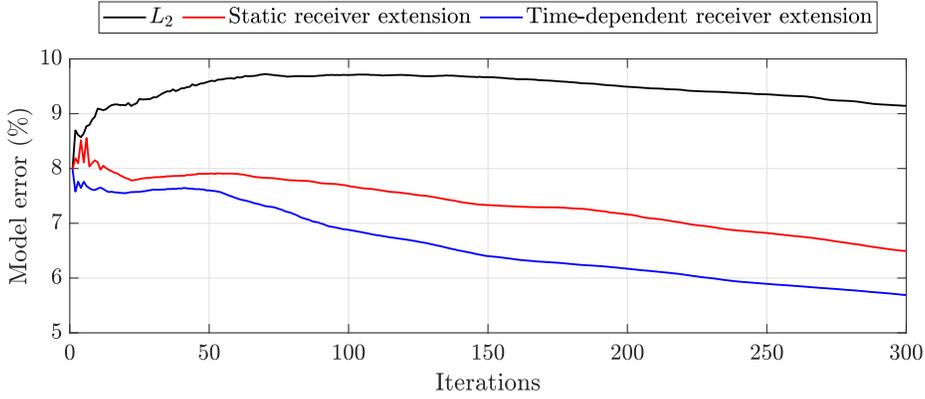


Figure 16: Receiver relocation as a function of iterations,(a): static extended-receiver FWI, (b): time-dependent FWI

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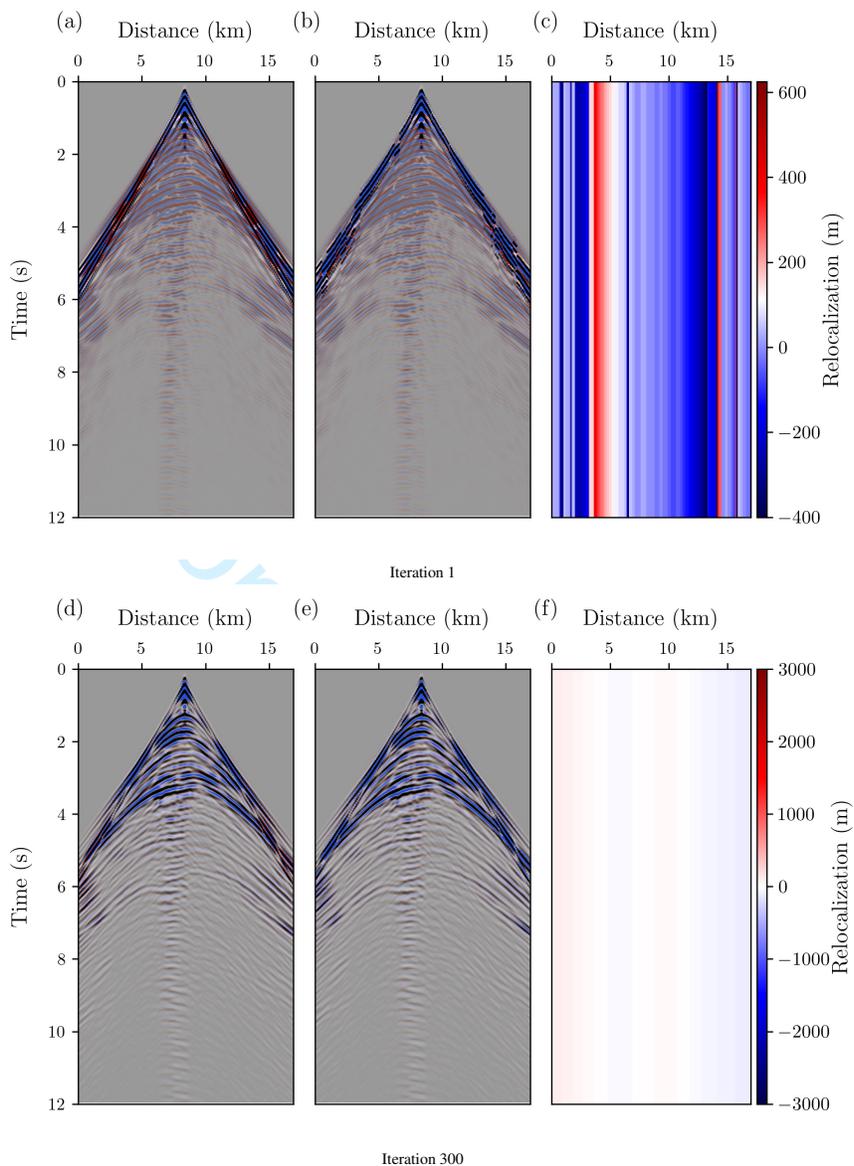


Figure 17: Synthetic and observed shot-gathers as well as the relocation gathers for the static case. We display the calculated data in a red and blue color scale while the observed data is shown in gray-scale. If solely blue and black are apparent on the wiggles, a good fit is obtained, if the red shows that the fit is not satisfactory. (a,d): Data fit before relocation, (b,e): data fit after relocation and (c,f): relocation gather, it has the same dimension as the shot gather. The first iteration is shown in the first row (a,b,c), and the last iteration is shown in the second (d,e,f).

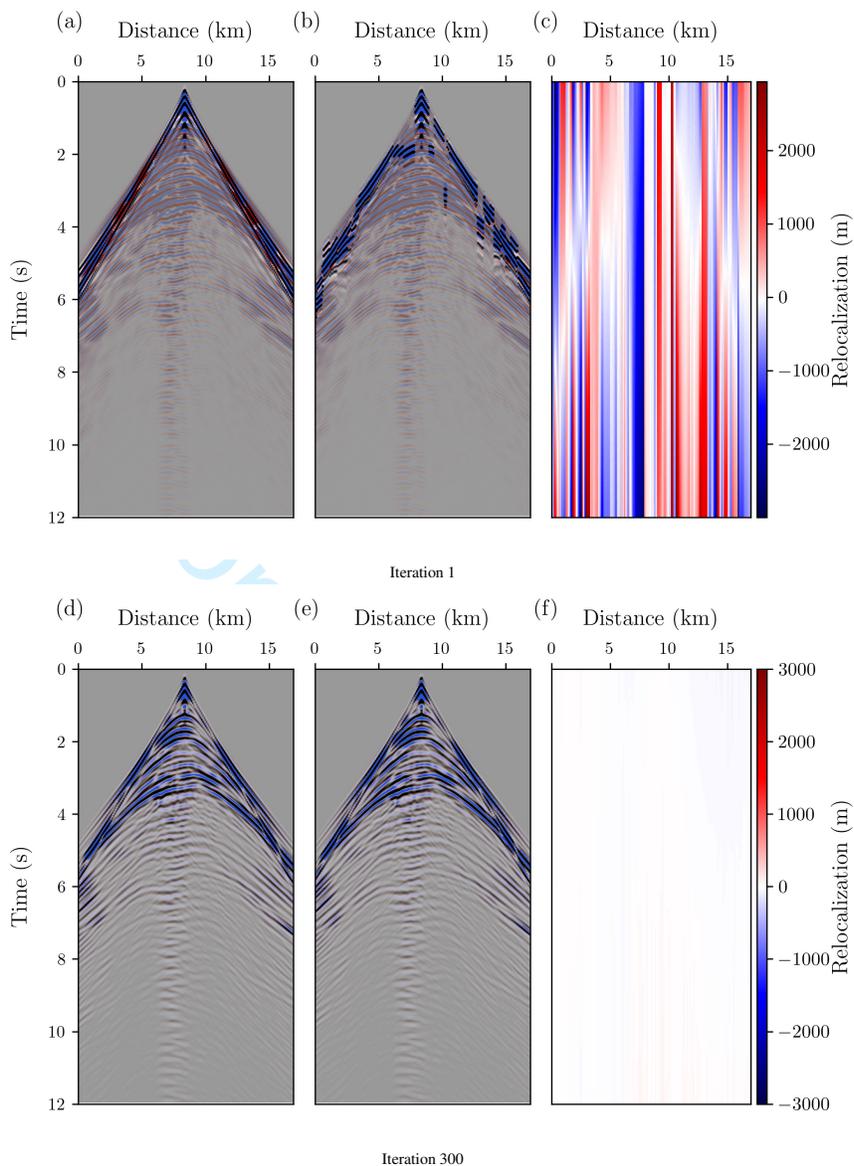


Figure 18: Synthetic and observed shot-gathers as well as the relocation gathers for the static case. We display the calculated data in a red and blue color scale while the observed data is shown in gray-scale. If solely blue and black are apparent on the wiggles, a good fit is obtained, if the red shows than the fit is not satisfactory. (a,d): Data fit before relocation, (b,e): data fit after relocation and (c,f): relocation gather, it has the same dimension as the shot gather. The first iteration is shown in the first row(a,b,c), and the last iteration is shown in the second (d,e,f).

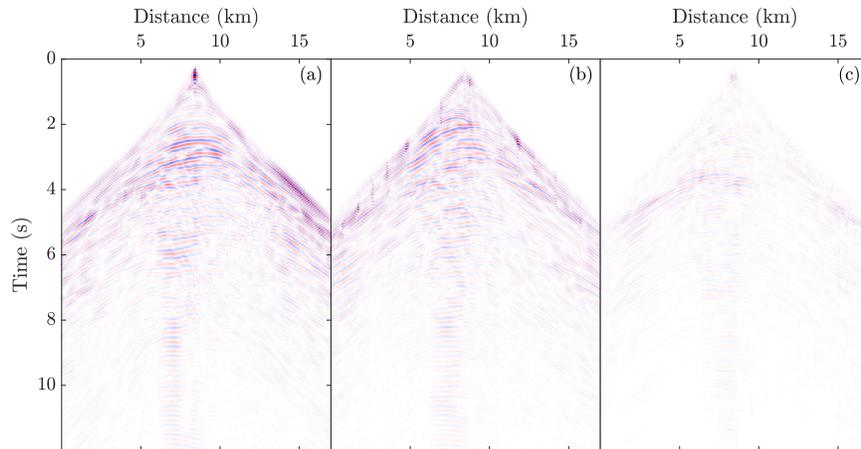


Figure 19: Adjoint source of the center shot point at the 300<sup>th</sup> iteration for (a): conventional FWI, (b): static receiver extension and (c): time-dependent receiver extension. The same color scale is used for all figures.

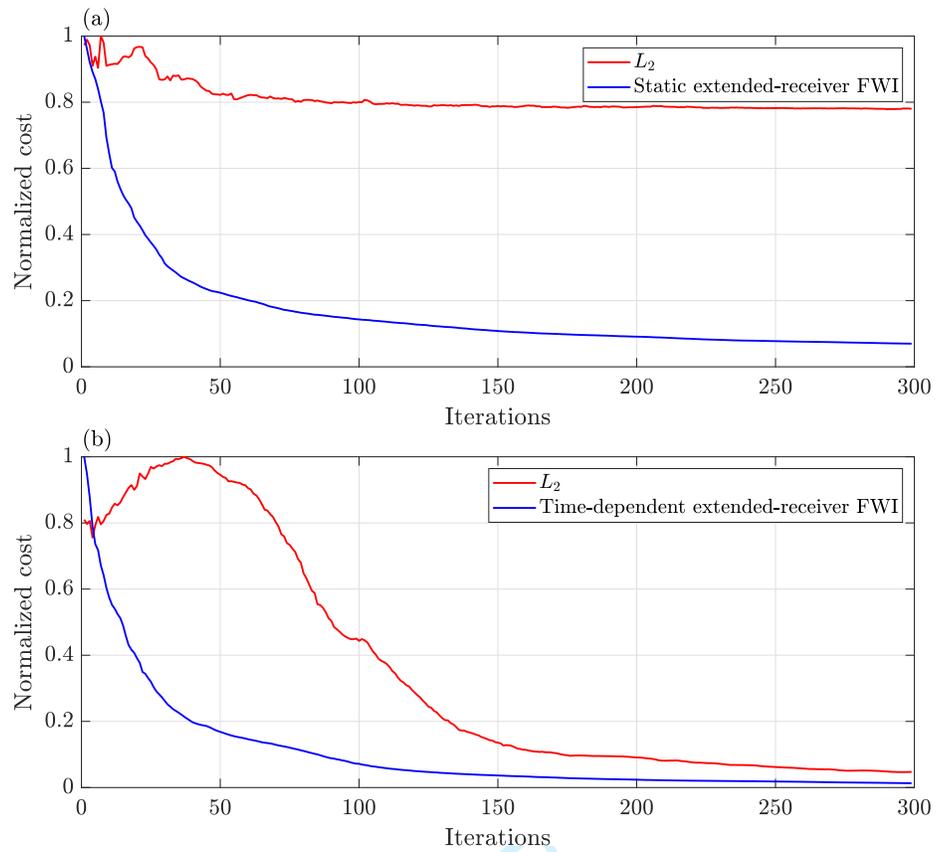


Figure 20: Cost function evolution as a function of iterations, extended-receiver FWI cost is plotted in black and the  $L_2$  norm of the data residuals at each iteration is shown in red. (a): static extended-receiver FWI, (b): time-dependent extended-receiver FWI.

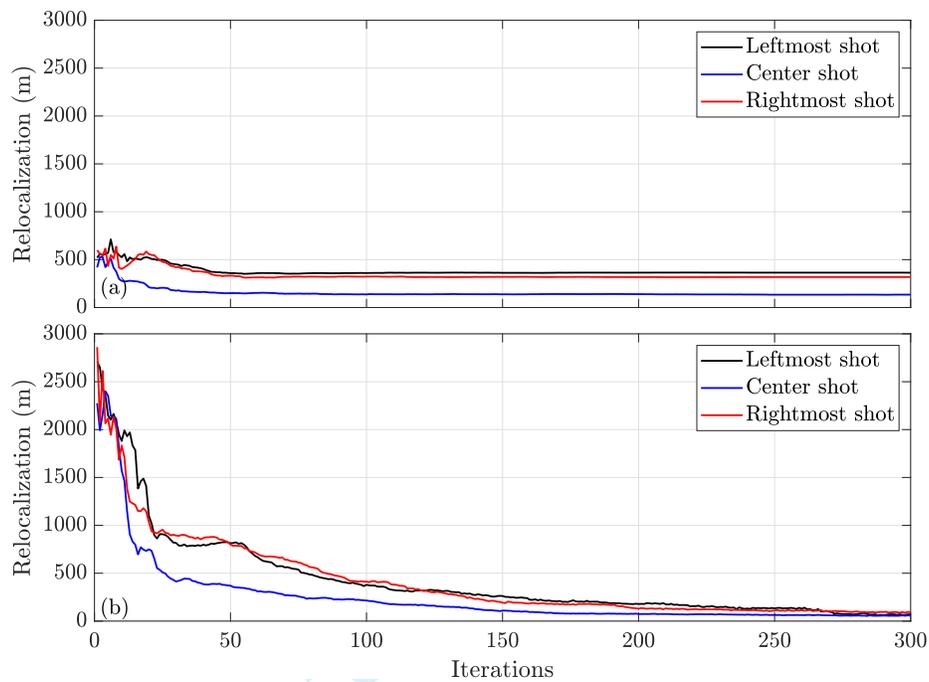


Figure 21: Receiver relocation as a function of iterations,(a): static extended-receiver FWI, (b): time-dependent FWI.

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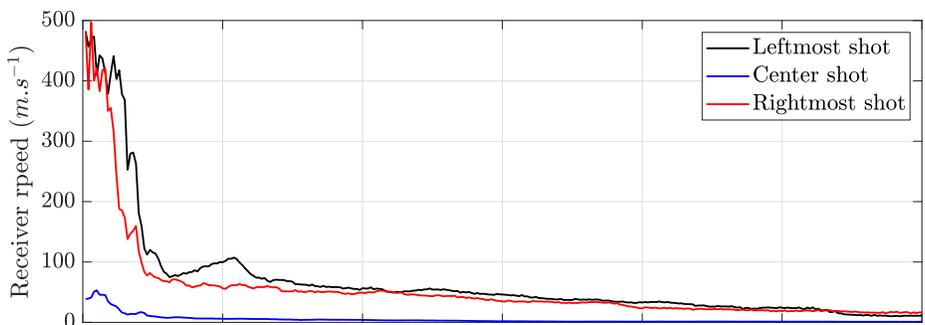


Figure 22: Receiver speed as a function of iterations for the time-dependent extended-receiver FWI.

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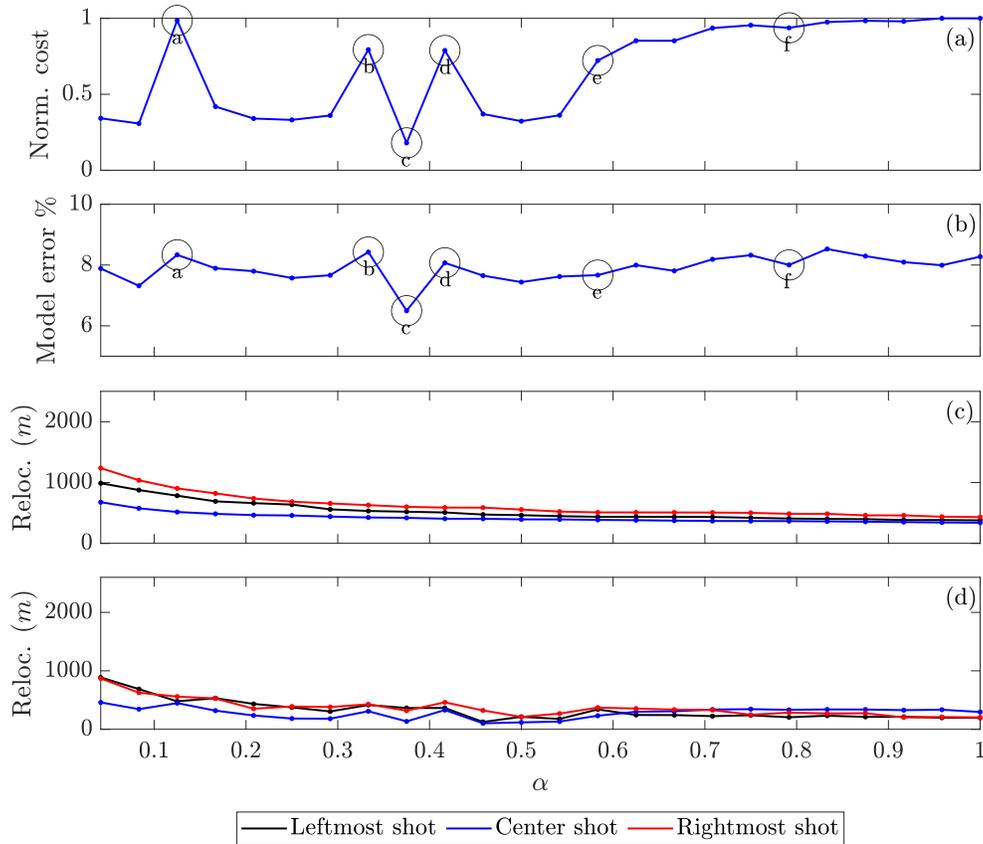


Figure 23: Tuning parameter  $\alpha$  impact on extended-receiver FWI with static relocalization. (a): normalized cost at the last iteration, (b): reconstructed model error, (c): relocalization at the first iteration and (d): relocalization at the last iteration. The lower two panels show plots for the leftmost, center and rightmost shot points. The black labeled circles in (a) and (b) correspond to selected  $\alpha$  values, whose corresponding final models are shown in Figure 24, where each model label correspond to an  $\alpha$  value with the same label.

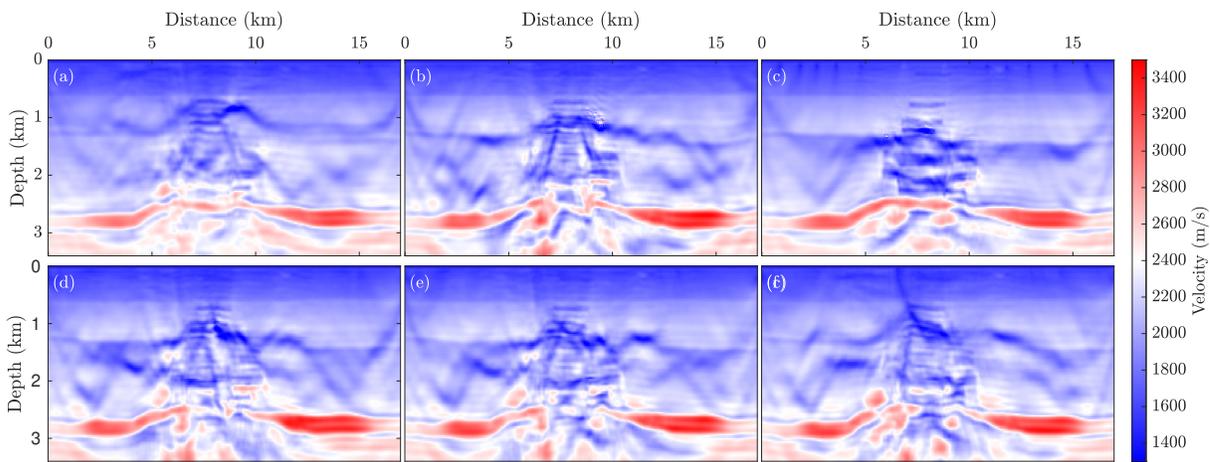


Figure 24: Tuning parameter  $\alpha$  impact on the velocity reconstruction using extended-receiver FWI with static relocation. (a):  $\alpha = 0.125$ , (b):  $\alpha = 0.333$ , (c):  $\alpha = 0.375$ , (d):  $\alpha = 0.4167$ , (e):  $\alpha = 0.5833$  and (f)  $\alpha = 0.7917$ . Each sub-figure label corresponds to an  $\alpha$  value indicated by black labeled circles in Figure 23a and 23b.

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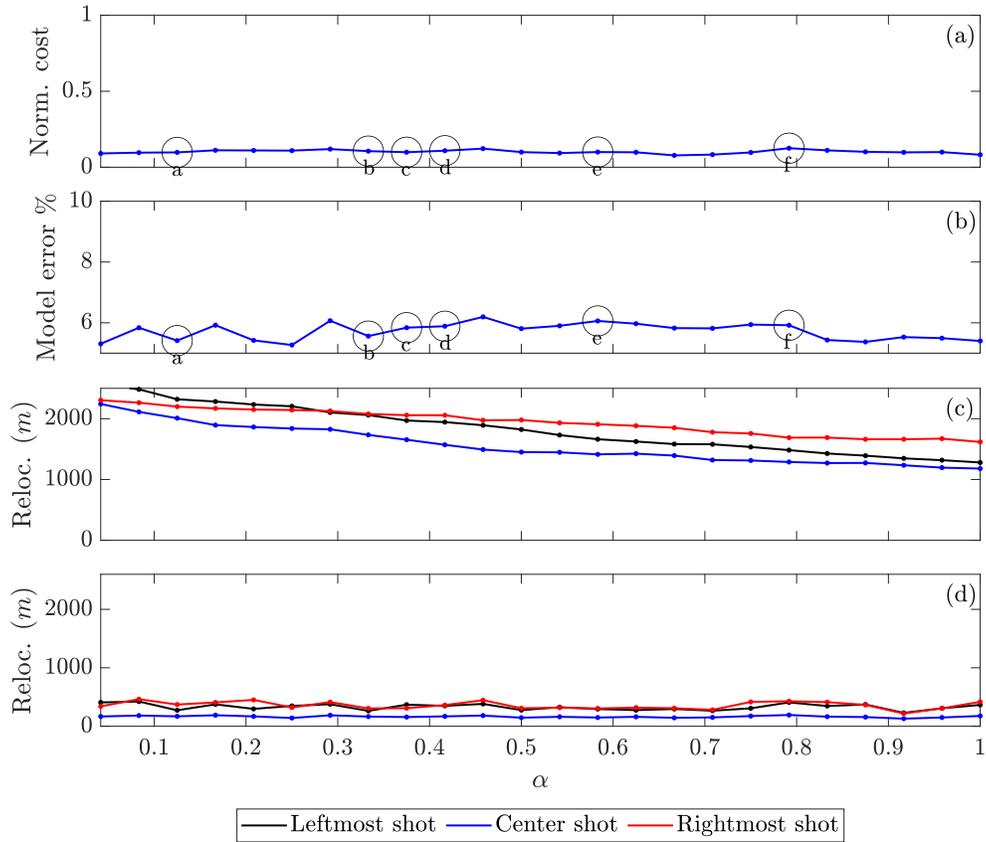


Figure 25: Tuning parameter  $\alpha$  impact on extended-receiver FWI with time-dependent relocalization. (a): normalized cost at the last iteration, (b): reconstructed model error, (c): relocalization at the first iteration and (d): relocalization at the last iteration. The lower two panels show plots for the leftmost, center and rightmost shot points. The black labeled circles in (a) and (b) correspond to selected  $\alpha$  values, whose corresponding final models are shown in Figure 26, where each model label correspond an  $\alpha$  value with the same label.

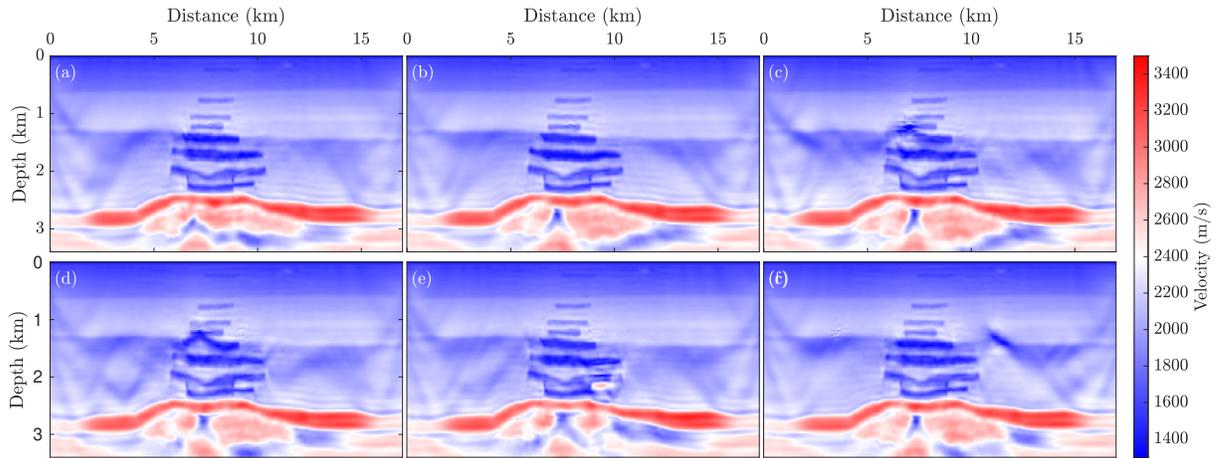


Figure 26: Tuning parameter  $\alpha$  impact on the velocity reconstruction using extended-receiver FWI with time-dependent relocalization. (a):  $\alpha = 0.125$ , (b):  $\alpha = 0.333$ , (c):  $\alpha = 0.375$ , (d):  $\alpha = 0.4167$ , (e):  $\alpha = 0.5833$  and (f)  $\alpha = 0.7917$ . Each sub-figure label corresponds to an  $\alpha$  value indicated black labeled circles in Figure 23a and 23b.

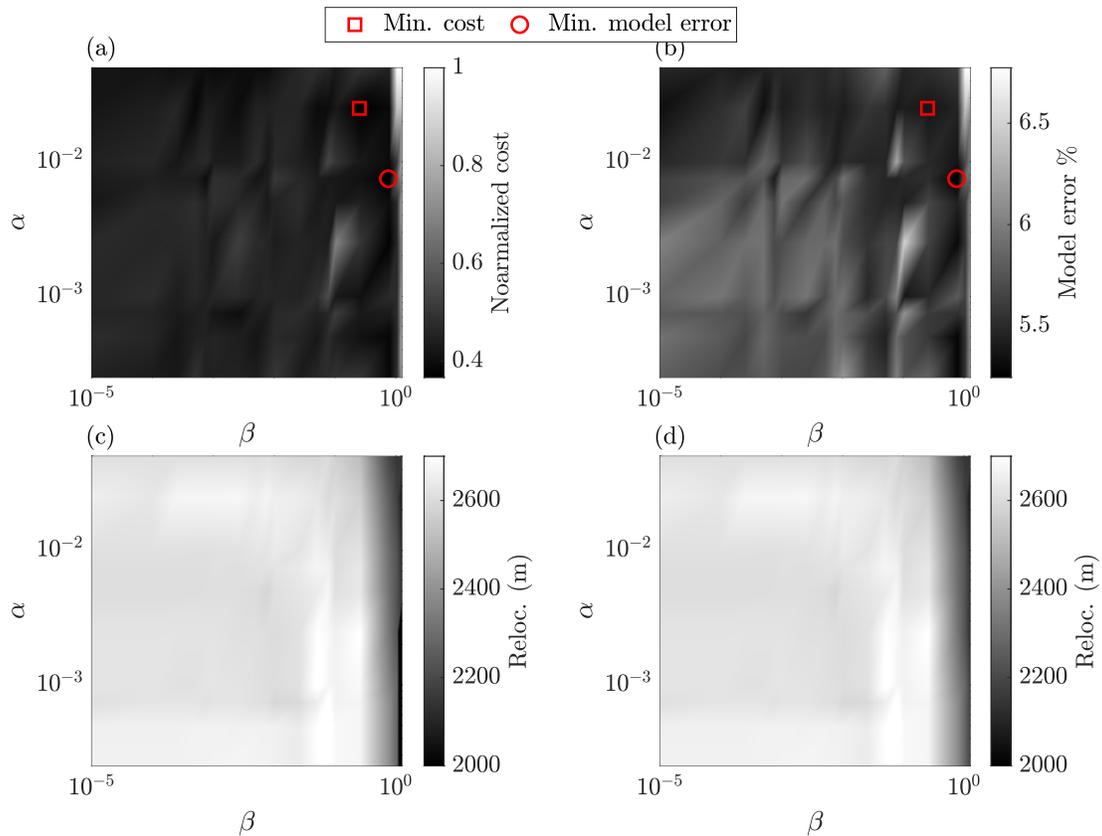


Figure 27: Tuning parameters impact on the (a): cost function at the last iteration, (b): model error and (c,d) receiver relocalization, shown here for (c) the leftmost and (d) the rightmost shot points.

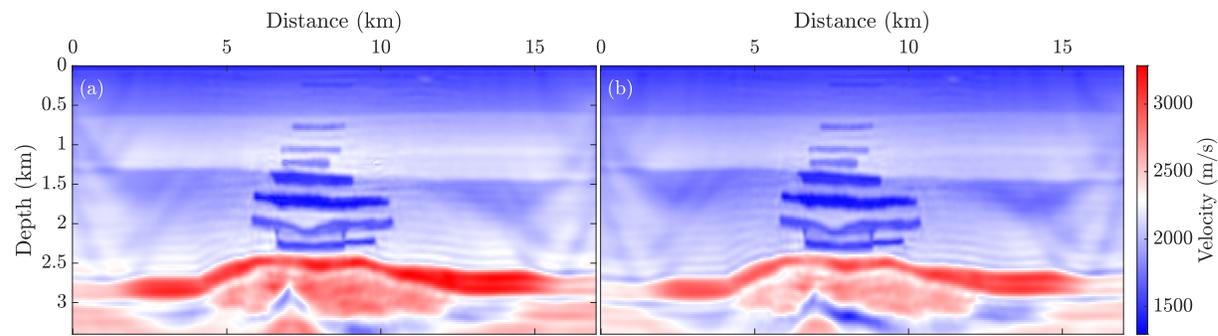


Figure 28: Reconstructed models corresponding to the (a): lowest cost and the (b): lowest model error (Figure 27).

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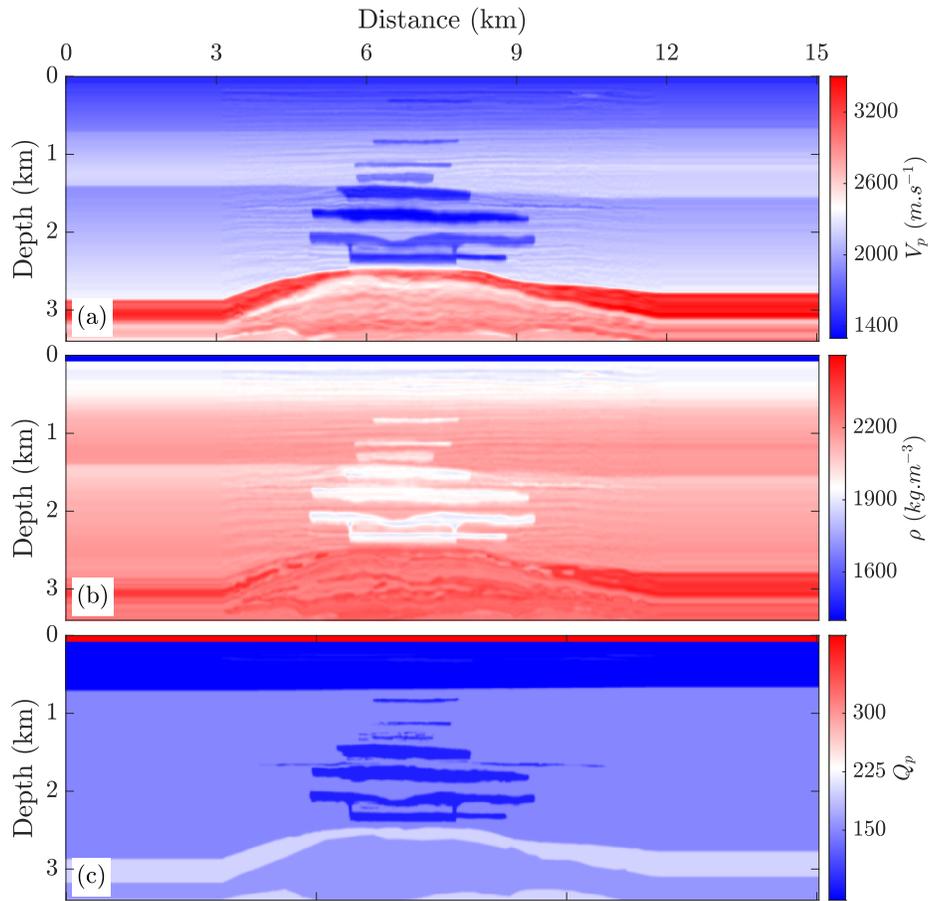


Figure 29: True models used to generate the observed data. (a): velocity, (b): density and (c): quality factor. The density and the quality factor in the water layer are  $1000 \text{ kg} \cdot \text{m}^{-3}$  and 1000, respectively. The color-bars in (b) and (c) are clipped for clarity, therefore, the color in the water layer is not representative of the true values.

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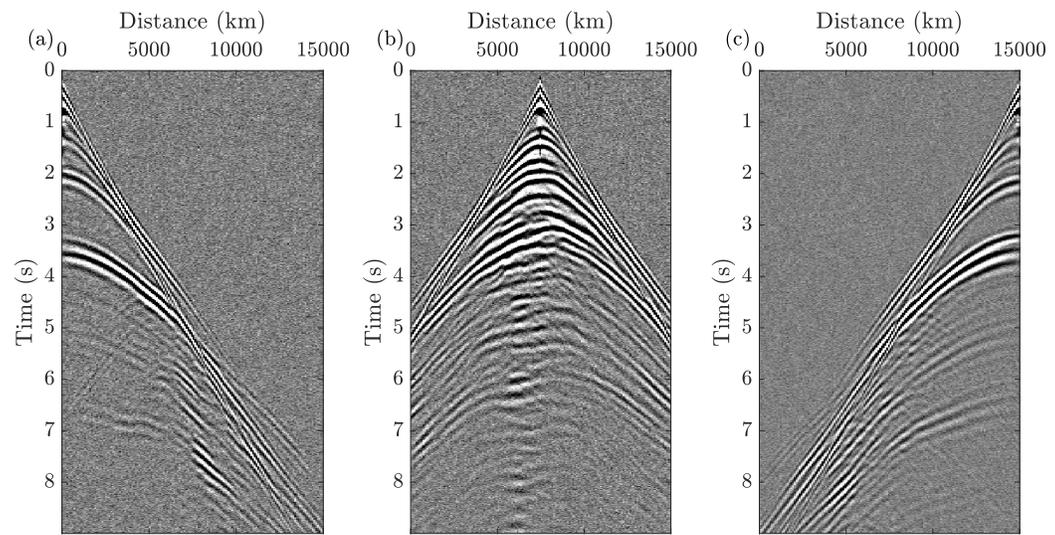


Figure 30: The observed data computed in a North Sea exploration scale synthetic model, (a) leftmost shot-gather, (b): center shot-gather and (c): rightmost shot-gather.

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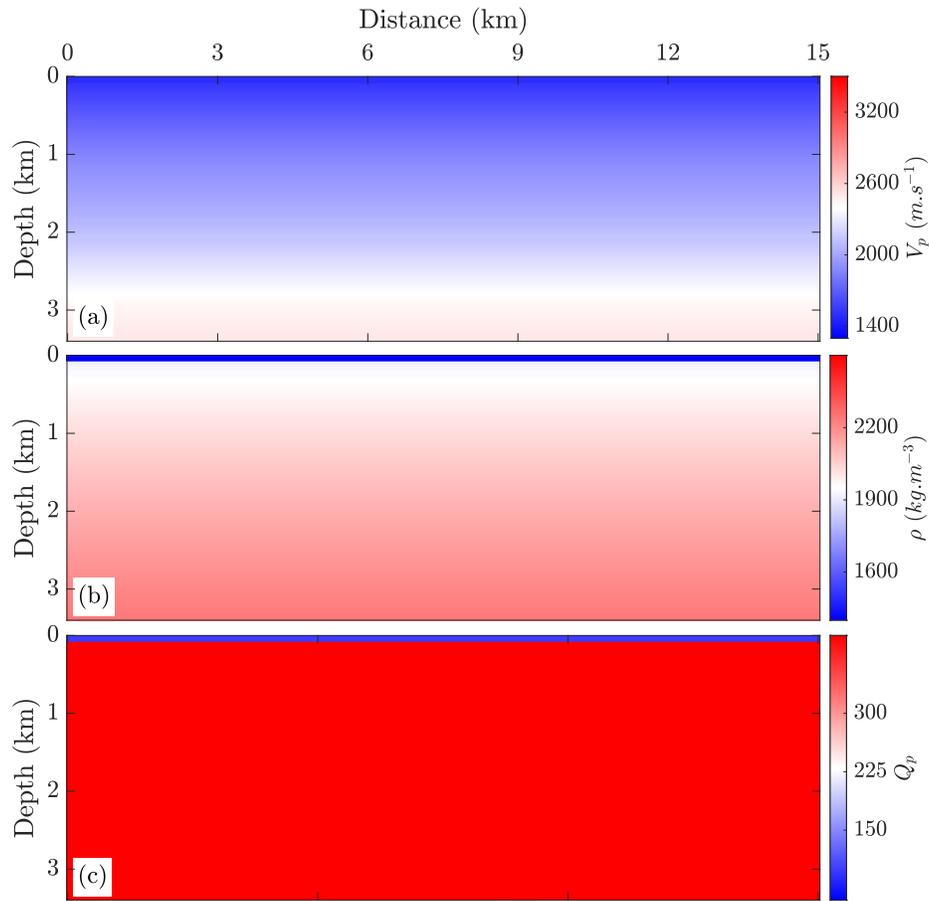


Figure 31: Starting models. (a): 1D velocity model, (b): density obtained using Gardner's law and (c): quality factor, set to 100 everywhere and 1000 in the water column. The color-bars in (b) and (c) are clipped for clarity, as a result, the color in the water layer is not representative of the true values.

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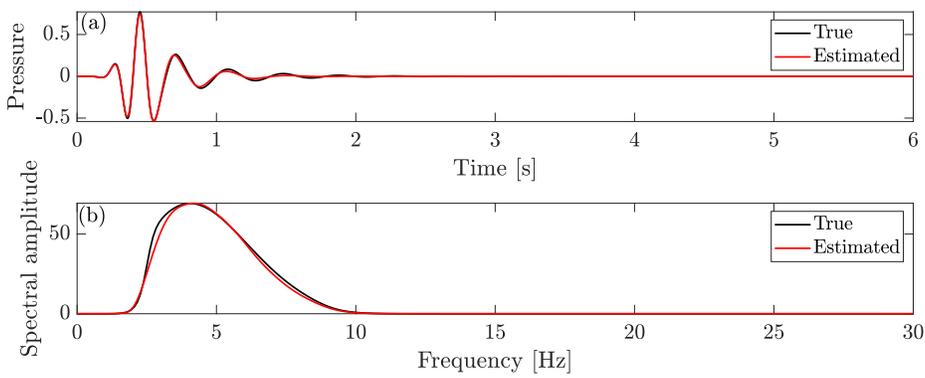


Figure 32: Source wavelet estimation in the starting velocity model. (a): source time function, (b): source frequency amplitude spectrum.

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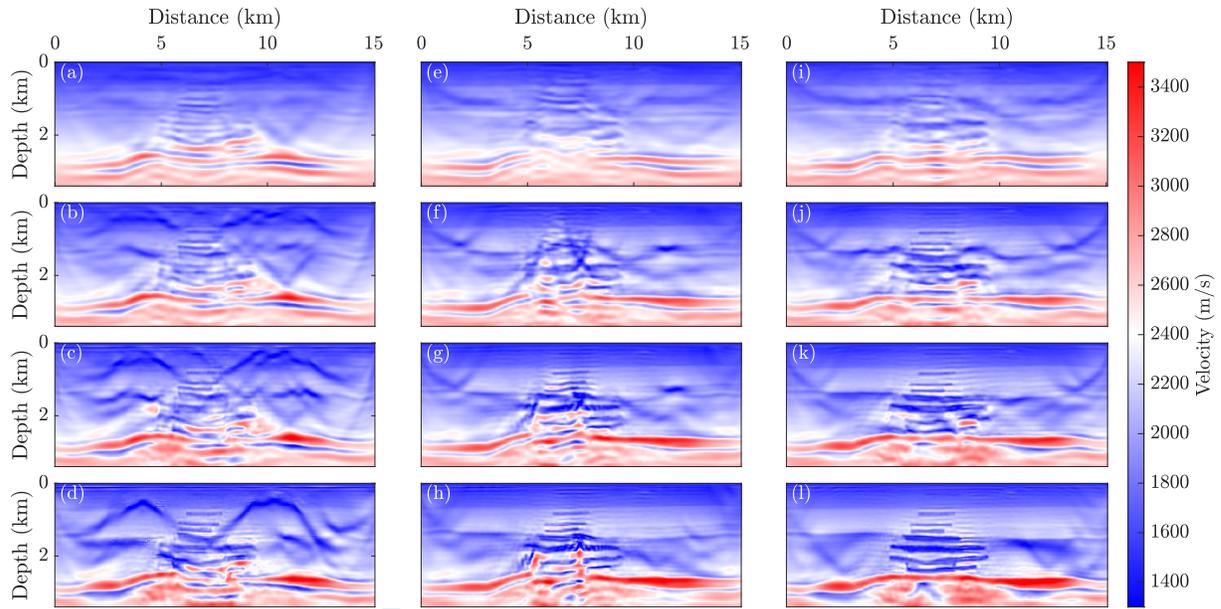


Figure 33: Reconstructed velocity models for (a-d) conventional FWI, (e-h) static receiver extension and (i-l): time-dependent receiver extension. This is shown for (a,e,i): 15 iterations, (b,f,j): 110 iterations (c,g,k): 205 iterations and (d,h,l) 300 iterations.

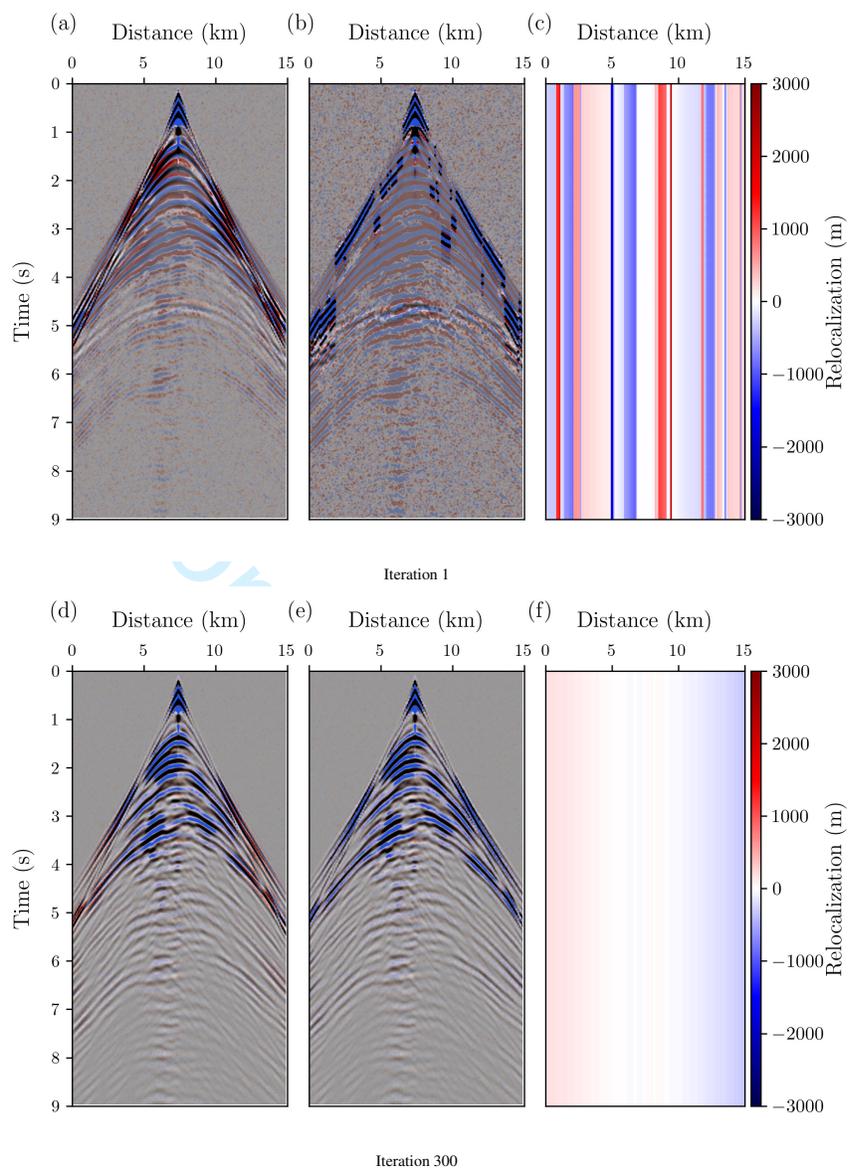


Figure 34: Synthetic and observed shot-gathers as well as the relocation gathers for the static case. We display the calculated data in a red and blue color scale while the observed data is shown in gray-scale. If solely blue and black are apparent on the wiggles, a good fit is obtained, if the red shows that the fit is not satisfactory. (a,d): Data fit before relocation, (b,e): data fit after relocation and (c,f): relocation gather, it has the same dimension as the shot gather. The first iteration is shown in the first row (a,b,c), and the last iteration is shown in the second (d,e,f).

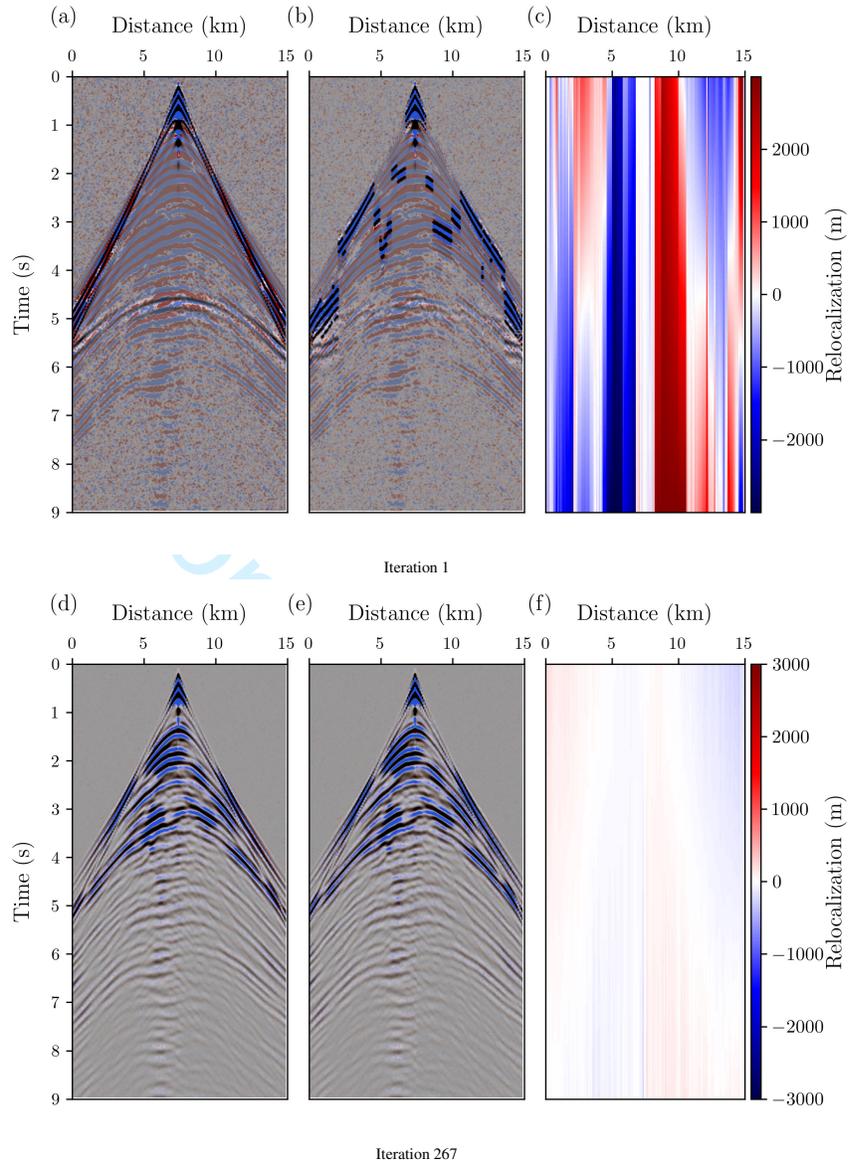


Figure 35: Synthetic and observed shot-gathers as well as the relocation gathers for the static case. We display the calculated data in a red and blue color scale while the observed data is shown in gray-scale. If solely blue and black are apparent on the wiggles, a good fit is obtained, if the red shows than the fit is not satisfactory. (a,d): Data fit before relocation, (b,e): data fit after relocation and (c,f): relocation gather, it has the same dimension as the shot gather. The first iteration is shown in the first row(a,b,c), and the last iteration is shown in the second (d,e,f).

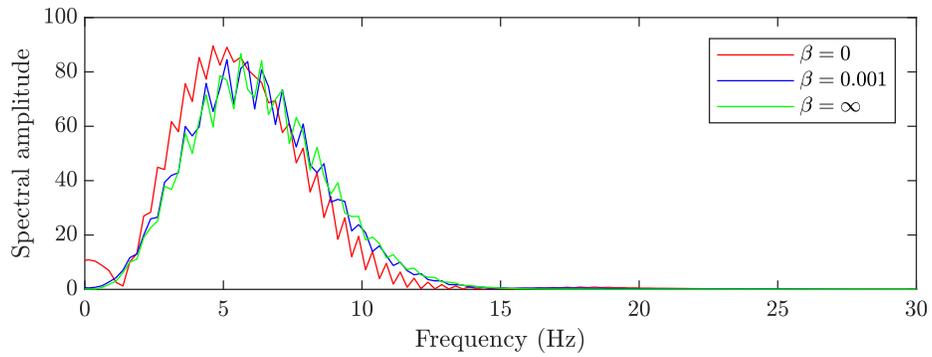


Figure 36: Calculated data amplitude spectrum for three cases: time-dependent relocation without the second penalty term ( $\beta = 0$ , shown in red) and with the second penalty term ( $\beta = 0.001$ ), as well as the static case ( $\beta = \infty$ ). The notches in the spectra are caused by the free-surface reflection.

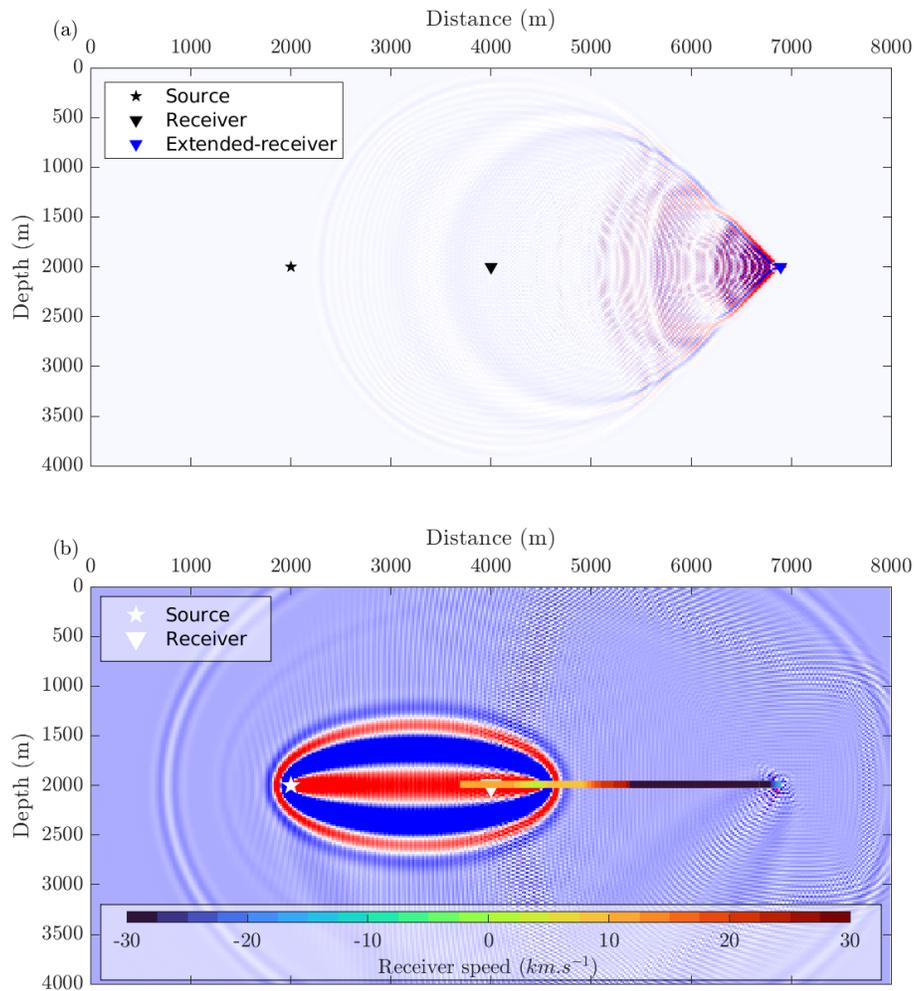


Figure 37: Gradient computation with  $\beta = 0$ . (a): adjoint field snapshot at 3.18 s, the extended receiver (adjoint source) is moving to the right causing the Mach cone shape in the wavefield, (b) extended receiver FWI kernel, the receiver positions are shown, the color indicates the receiver speed.

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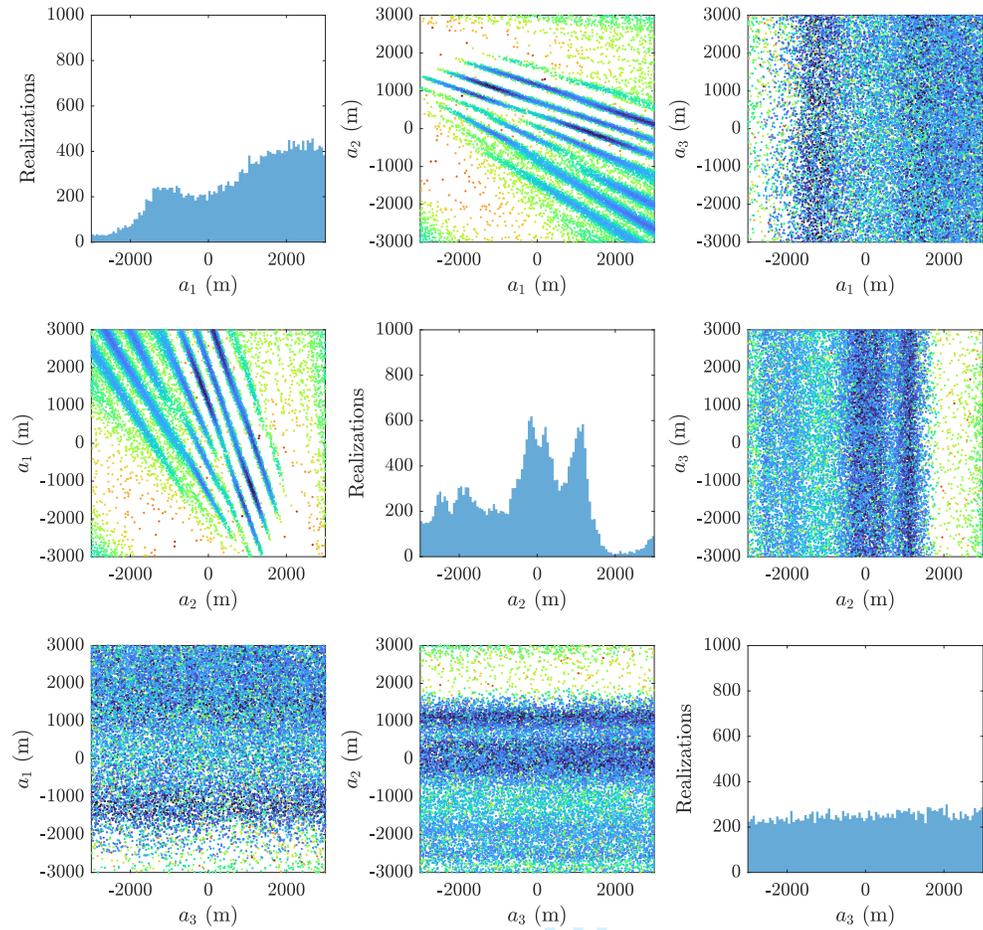


Figure 38: MCMC sampling of the inner misfit function, samples of each degree of freedom are cross-plotted against another, the color map indicates the value of the cost function. The plots on the diagonal show the histograms of samples of each degree of freedom.

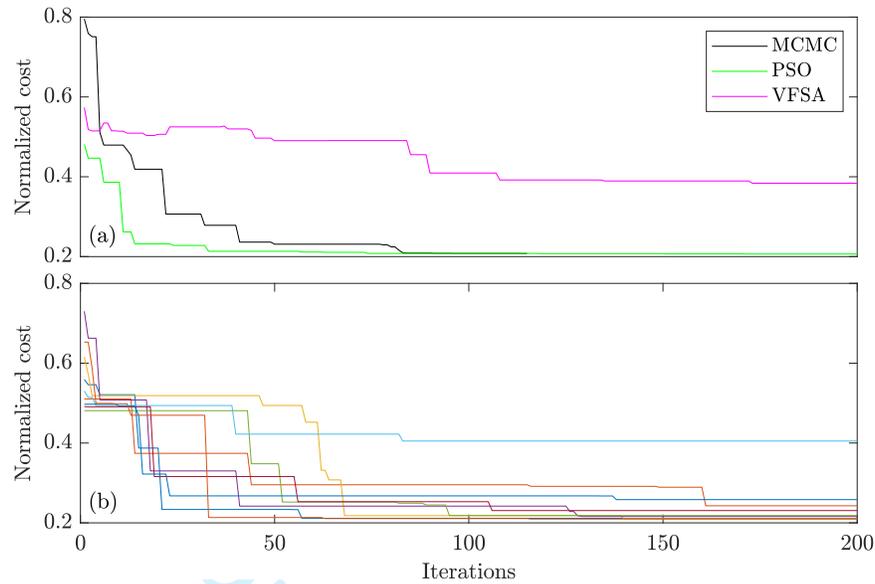


Figure 39: Cost function values as a function of inner-loop iterations for one receiver. (a): McMC candidates that lower the cost functions are shown in black, PSO global-best cost is shown in green, and Very Fast Simulated Annealing best solutions are shown in magenta. (b): the personal-best cost function of few particles as a function of iterations.

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**LIST OF TABLES**

1179	1	$\alpha$ and $\beta$ values we use for the parametric study. The first row shows the values considered for both $\alpha$ and $\beta$ , while the second row shows the additional values we test only for $\beta$ . . . . . 104
1182	2	CPU times in seconds for the different steps of the computation. . . . . 105

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$\alpha, \beta$	0.0003	0.0005	0.0008	0.001	0.002	0.005	0.0075	0.01	0.025	0.05		
$\beta$	0.0025	0.005	0.0075	0.01	0.025	0.0500	0.075	0.1	0.25	0.75	1.	1.25

Table 1:  $\alpha$  and  $\beta$  values we use for the parametric study. The first row shows the values considered for both  $\alpha$  and  $\beta$ , while the second row shows the additional values we test only for  $\beta$ .

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	Forward	Inner loop	Inner loop per receiver	Adjoint simulation+ gradient summation
Conventional FWI	17.6	-	-	66.4
Static	21.9	2.1	$1.4 \times 10^{-2}$	70.2
Time-dependent	22.1	53.7	0.3	74.6

Table 2: CPU times in seconds for the different steps of the computation.

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